

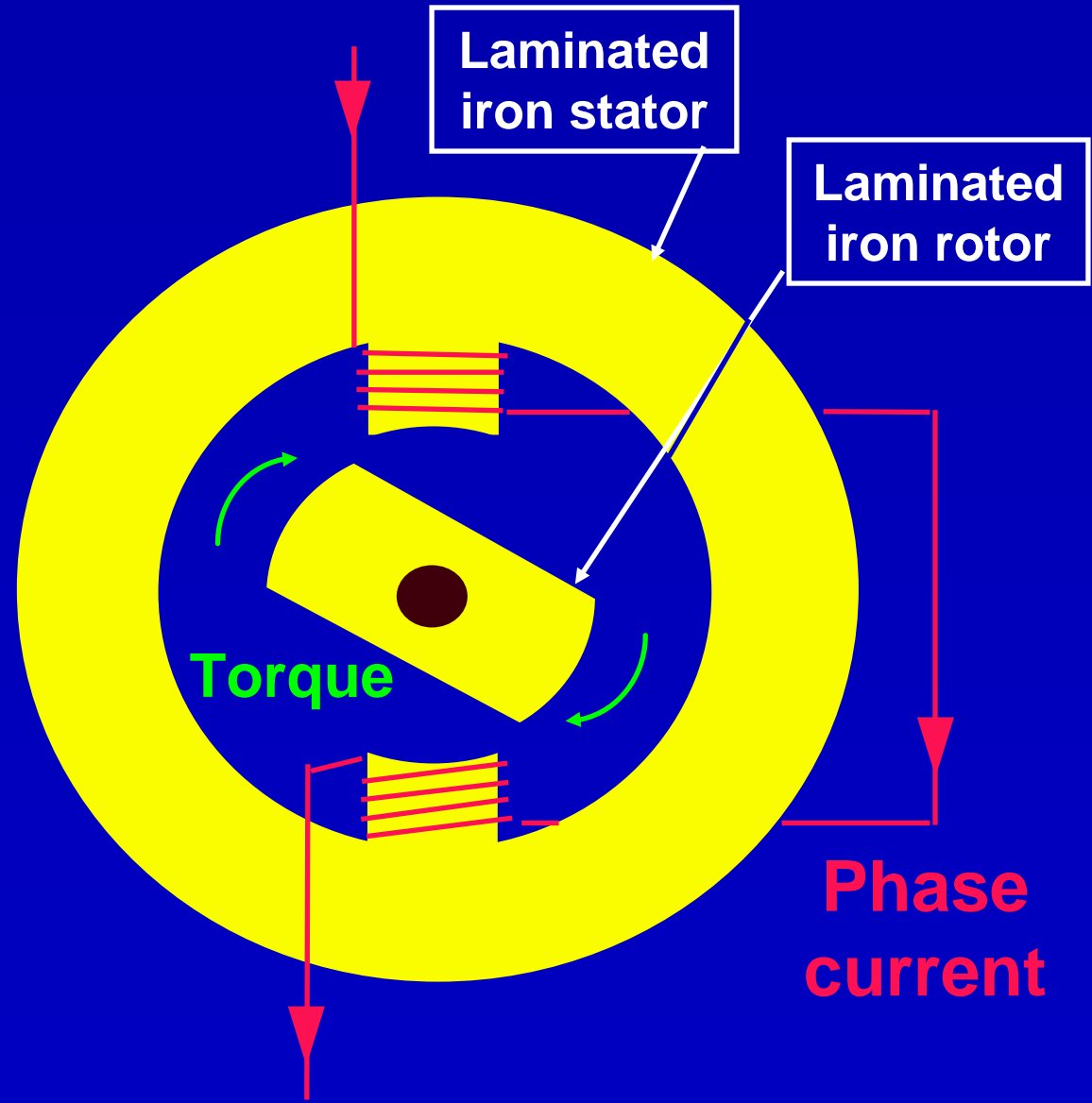


S R Drives®

***an introduction to switched reluctance
motors and controls***

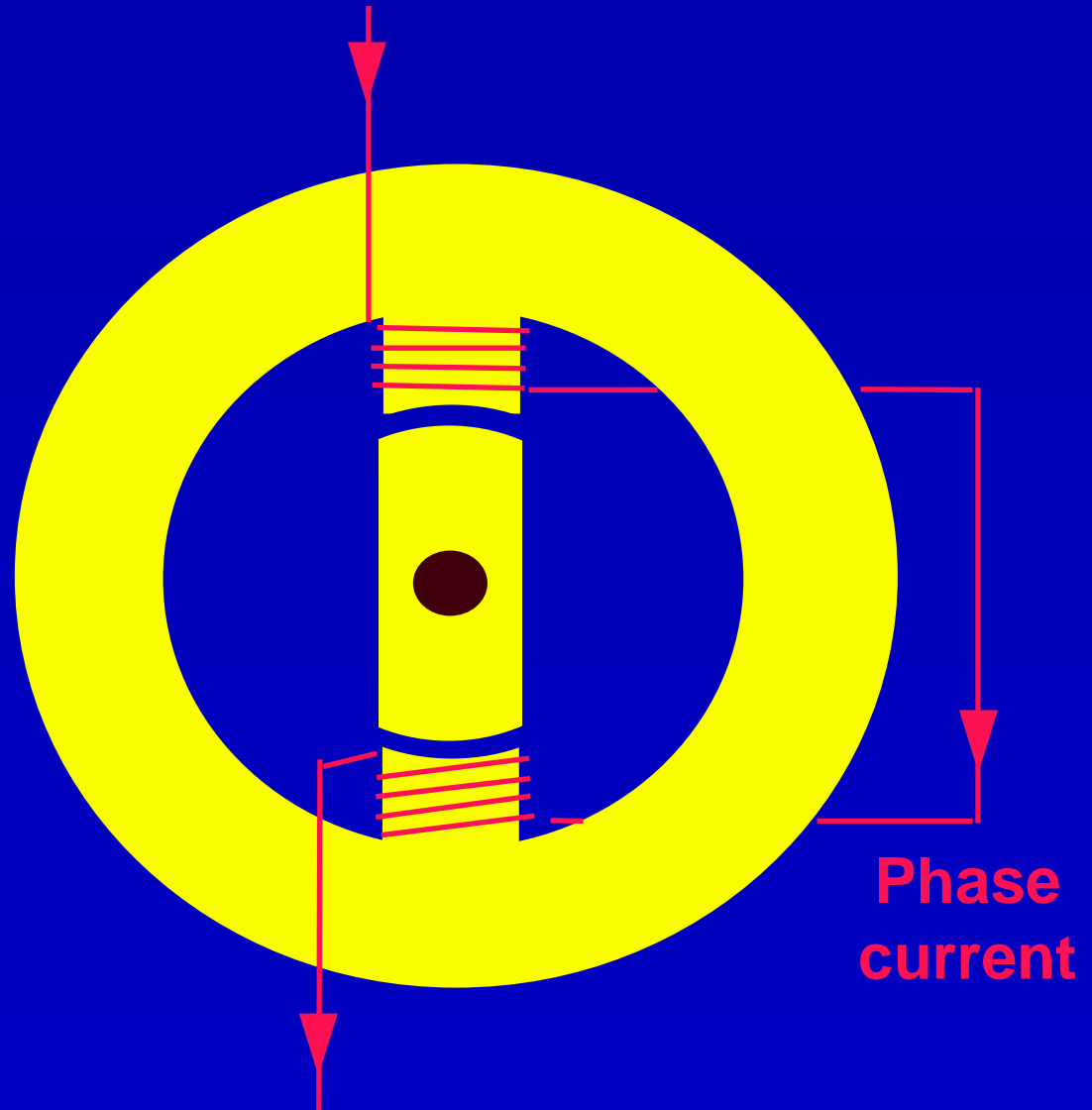
How does it work?

- Consider simple, single-phase, motor
- Phase current sets up magnetic flux in stator
- Magnetic attraction will try to turn rotor to its fully-aligned position
- Clock-wise torque will be produced (green arrows)
- This is the principle of a “variable reluctance motor”



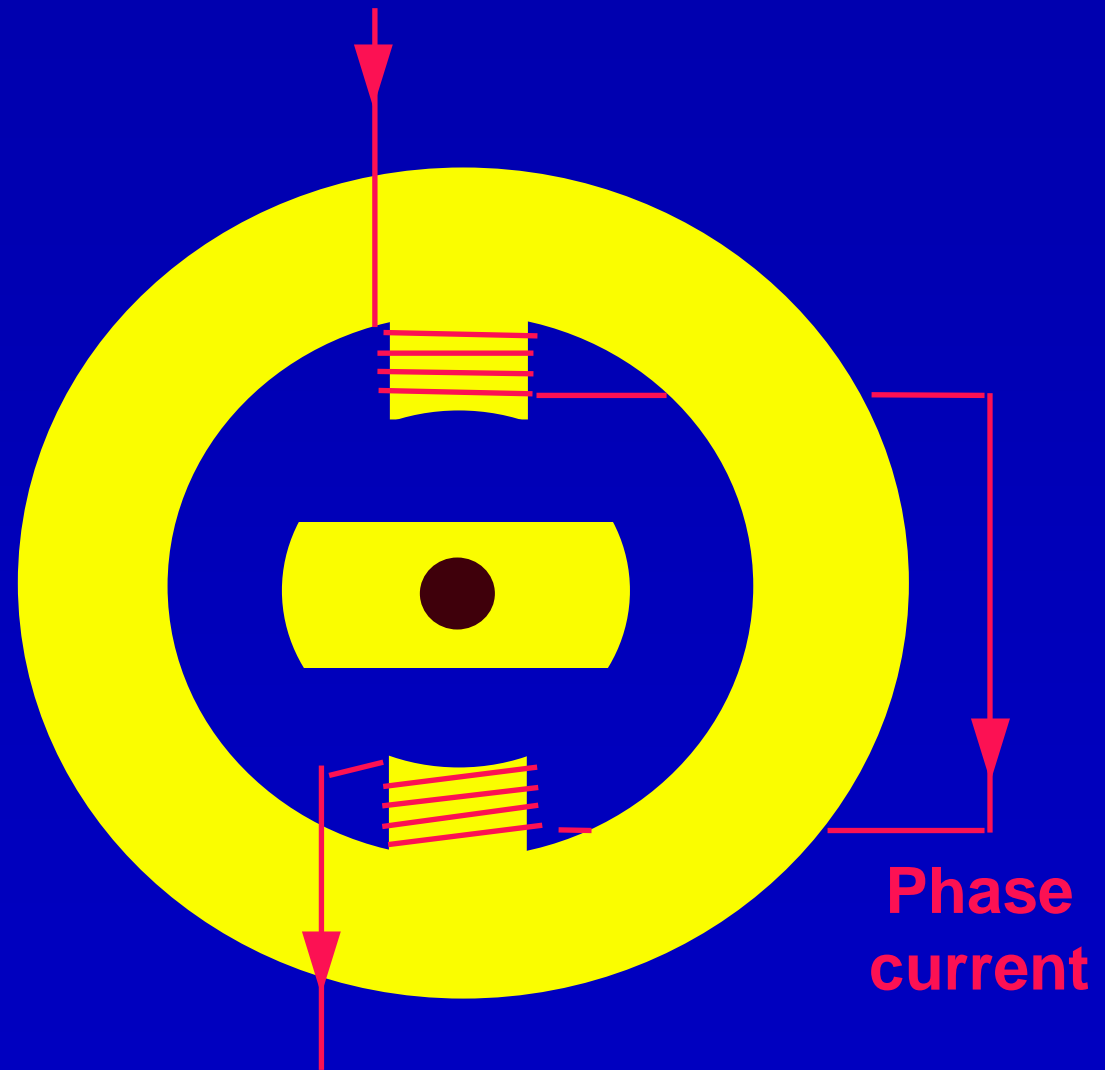
Phase torque is zero at fully aligned position

- Rotor position shown gives minimum magnetic circuit “reluctance”
- Phase inductance is at its maximum (L_{\max})
- This position often called “top dead centre” (TDC)



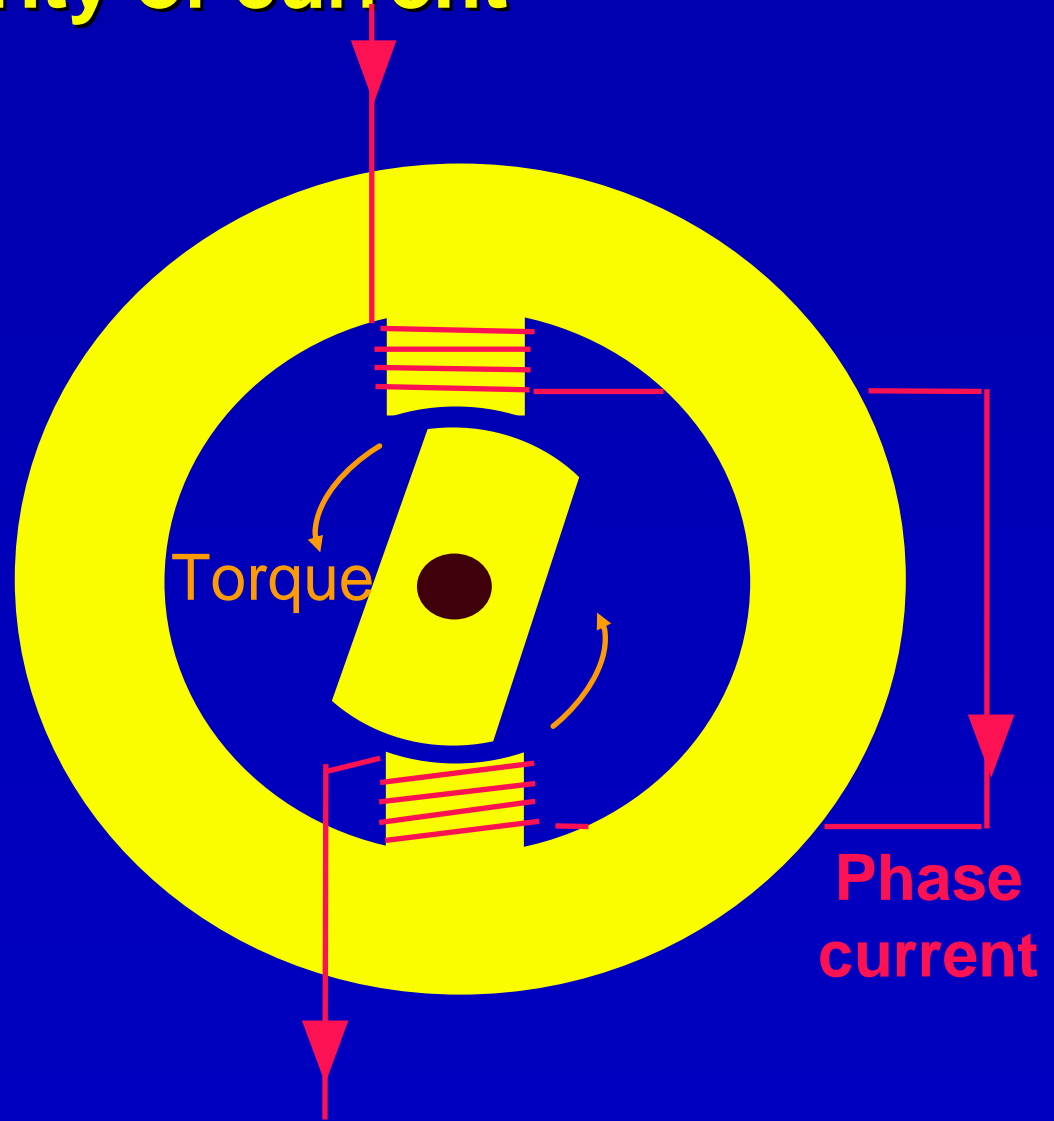
Zero torque also at fully un-aligned position

- Rotor position now yields maximum magnetic circuit reluctance
- Phase's electrical inductance will be at a minimum (L_{\min})
- Position often called “bottom dead centre” (BDC)



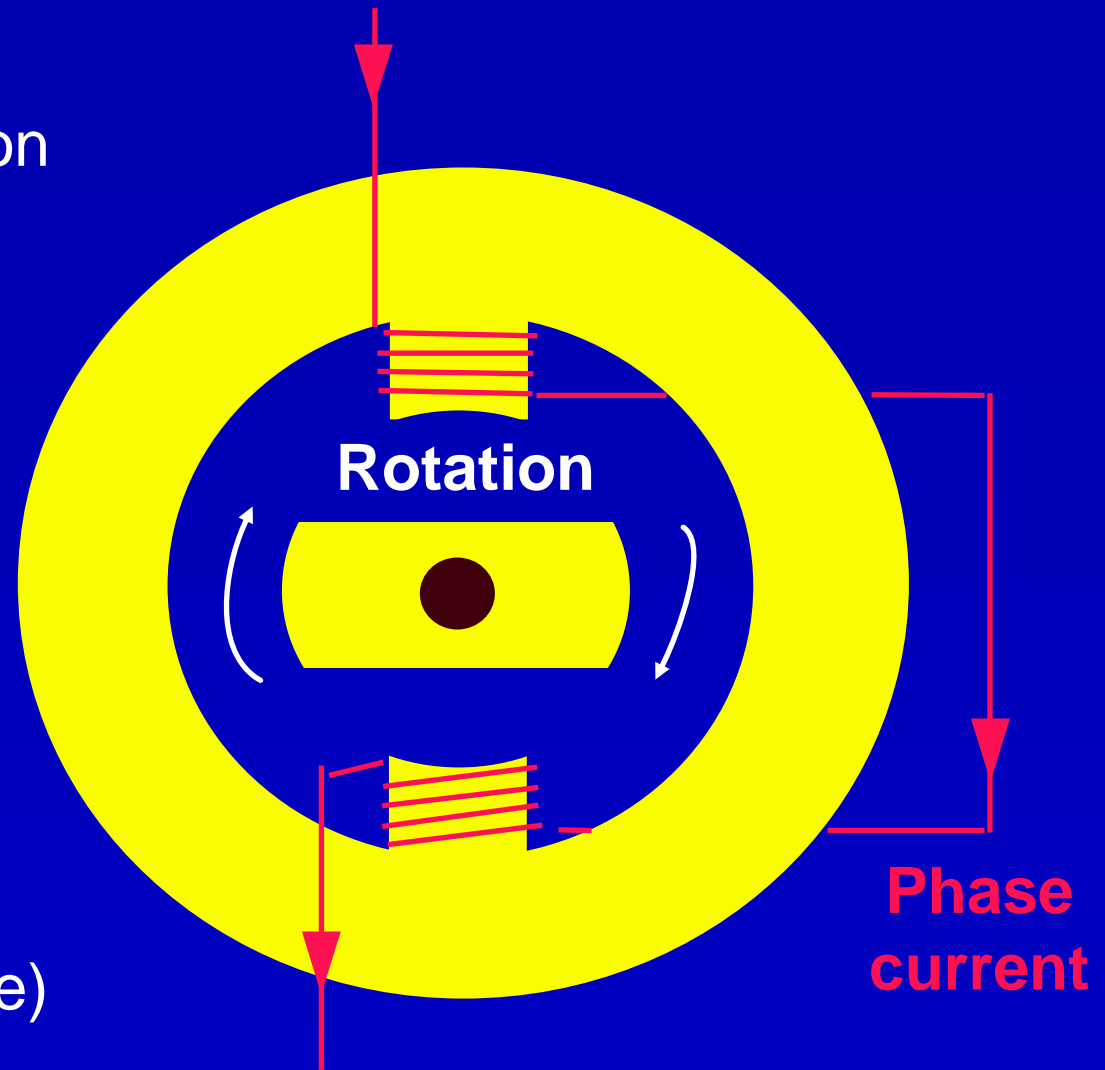
Torque can be reversed without changing polarity of current

- If phase current still flows in the interval after TDC, and before BDC is again reached, anti-clockwise torque will be produced (*orange arrows*)
- If the rotor is still rotating clockwise, this torque is BRAKING the load
- Positive or negative torque obtainable, simply by altering timing of winding excitation



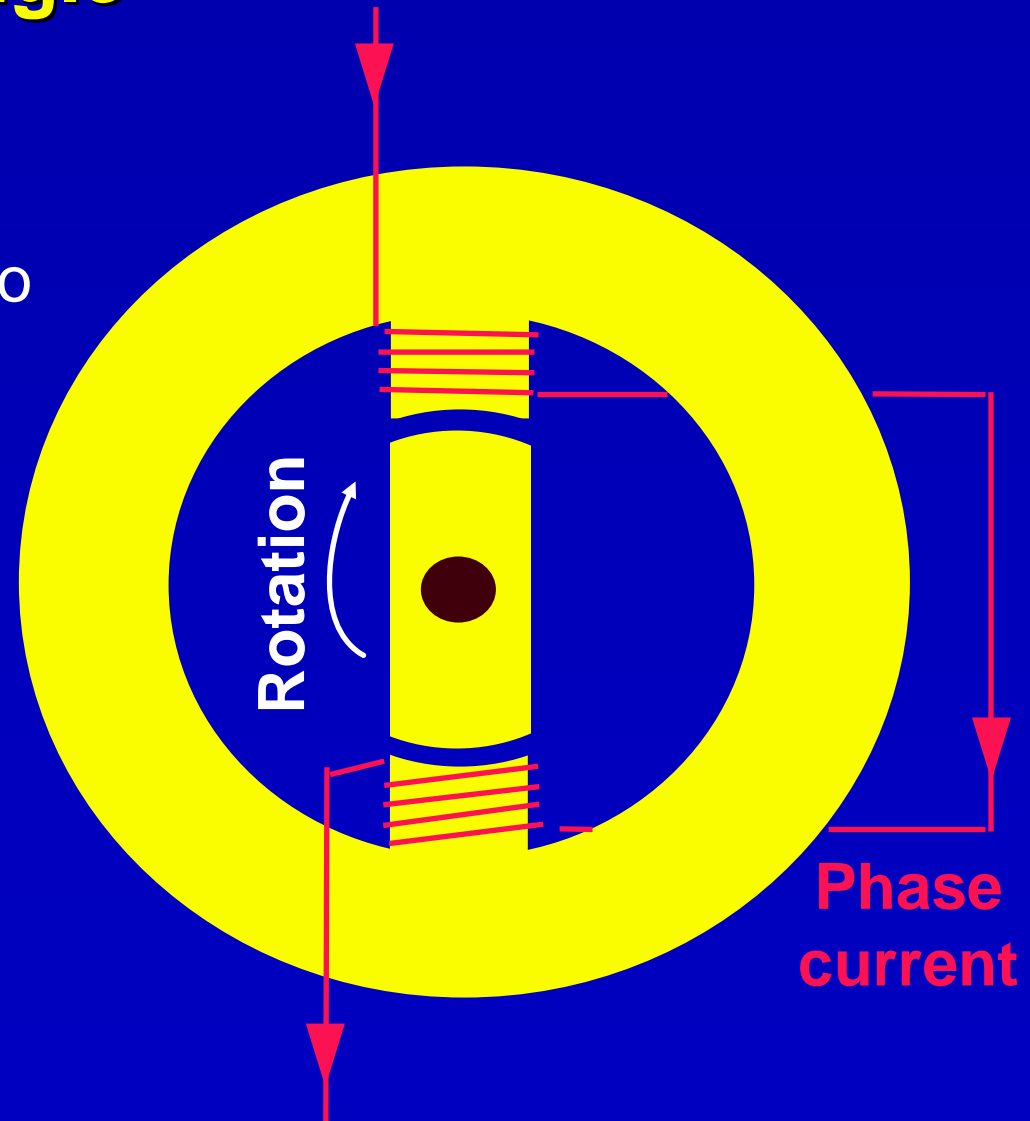
Operation as a switched reluctance motor

- Assume CLOCKWISE rotation
- Rotor is shown at BDC
- Get clockwise torque once rotor has turned past BDC
- If we switch phase on before BDC, we will get anti-clockwise torque
- So: ideally switch on at BDC – but not before!
(to maximise motoring torque)



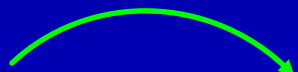
De-energising at the correct rotor angle

- When TDC is reached, the instantaneous torque falls to zero
- Get anti-clockwise braking torque when the rotor turns past TDC -- unless we switch phase current off
- (Ideally) switch off at TDC to maximise motoring torque

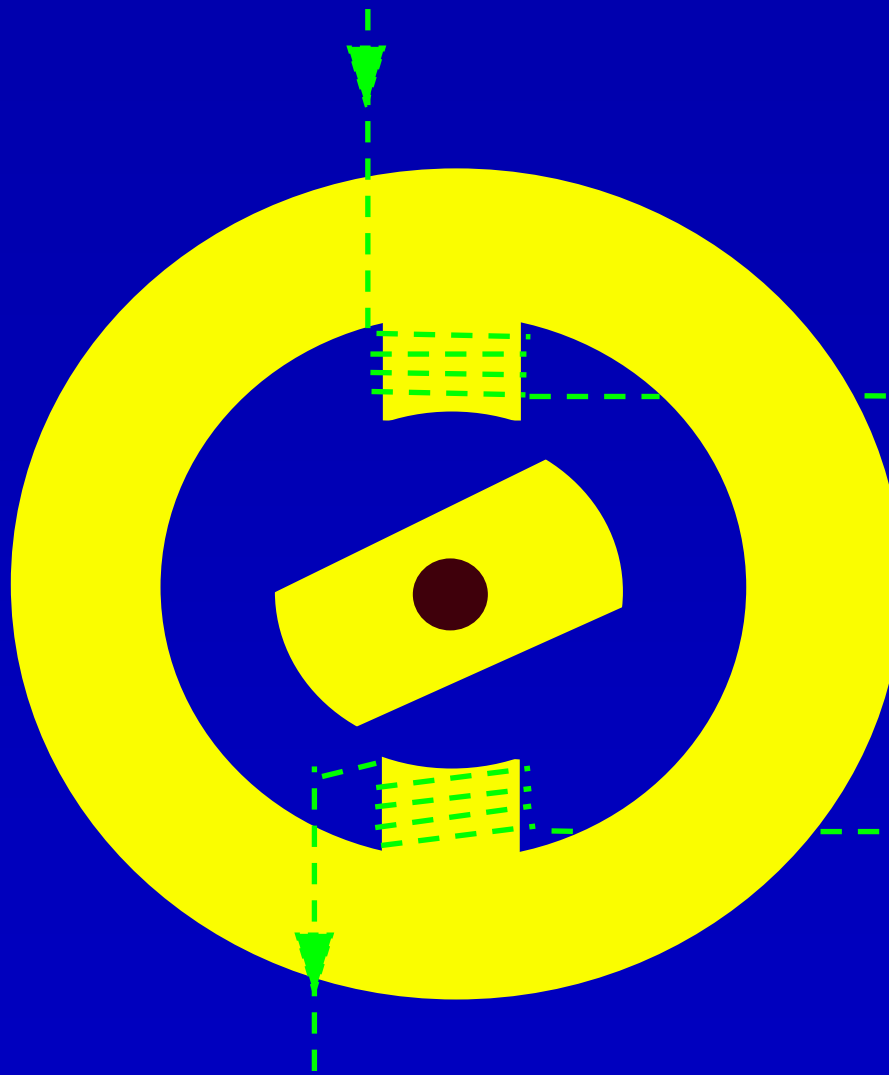


Simple animation of motoring operation follows...

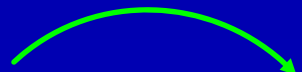
- Clockwise rotation assumed
- Switch on at bottom dead centre
- Switch off at top dead centre


CW
rotation

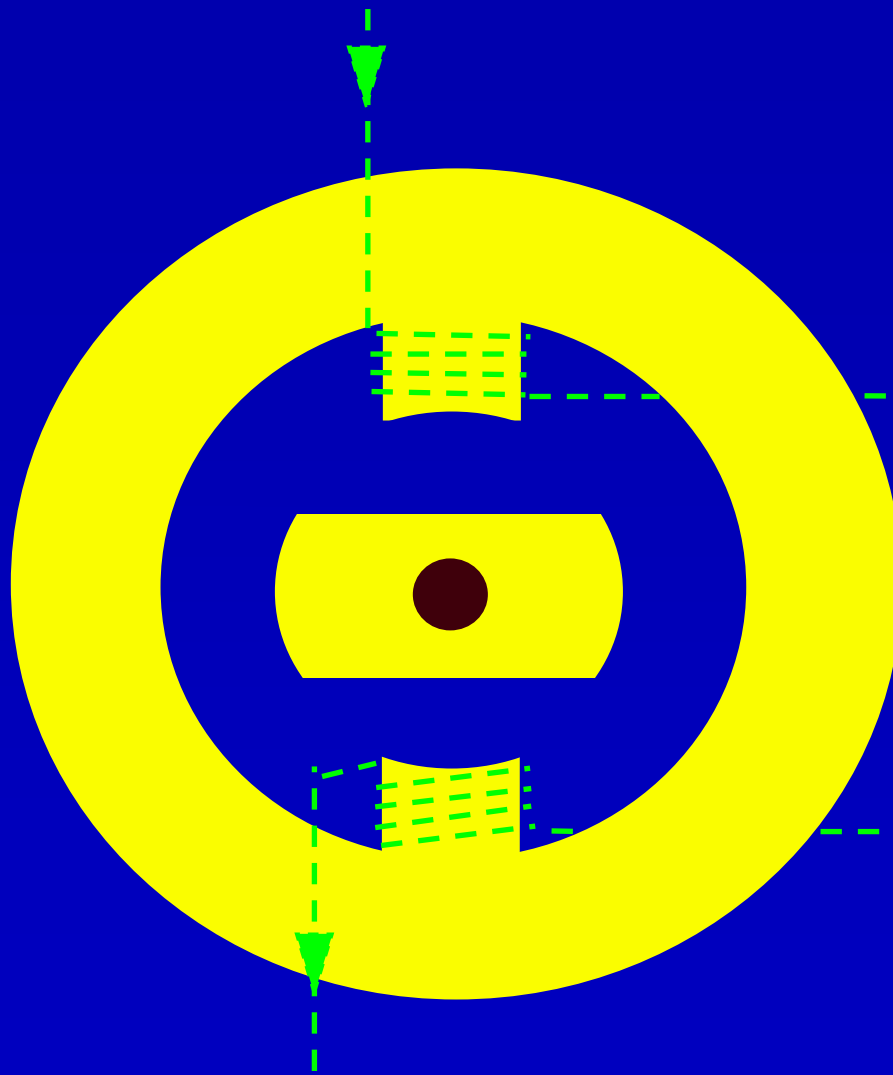
No
torque



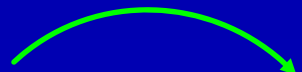
Phase
current
= ZERO


CW
rotation

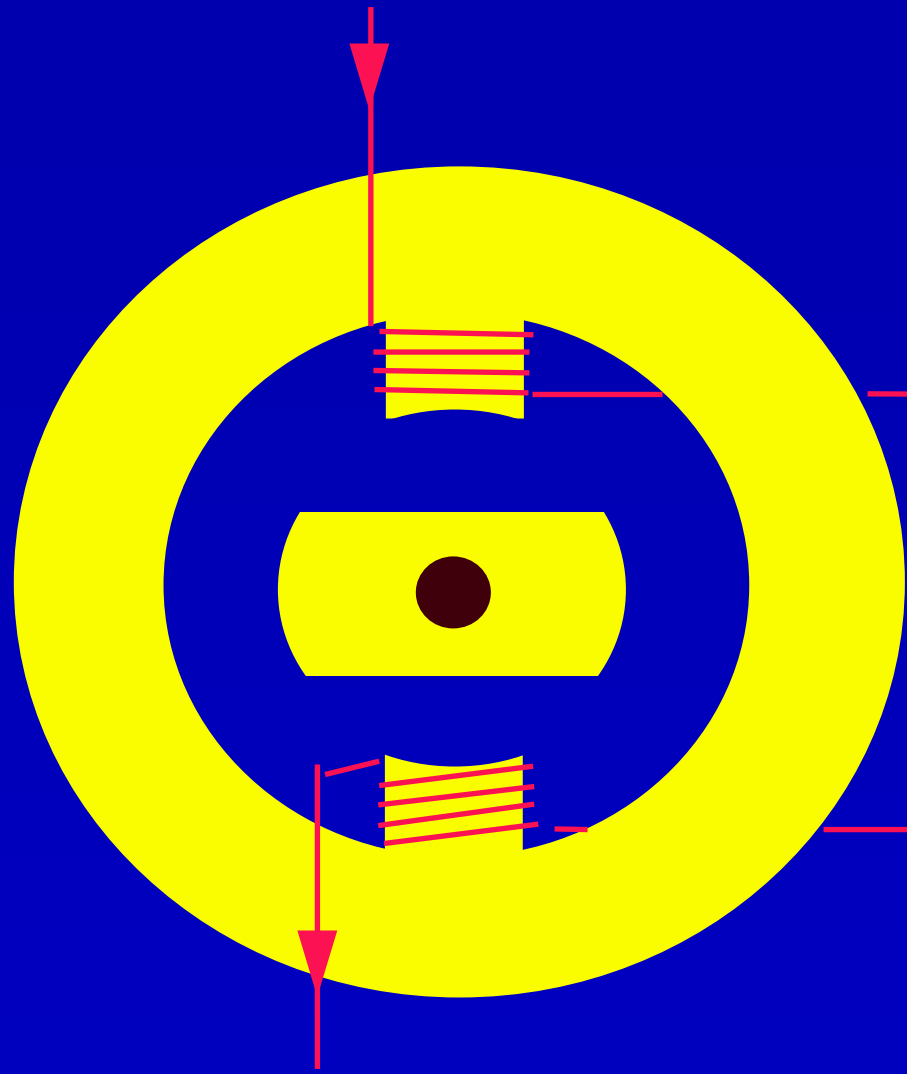
No
torque



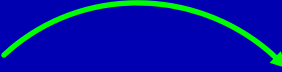
Phase
current
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CW
rotation

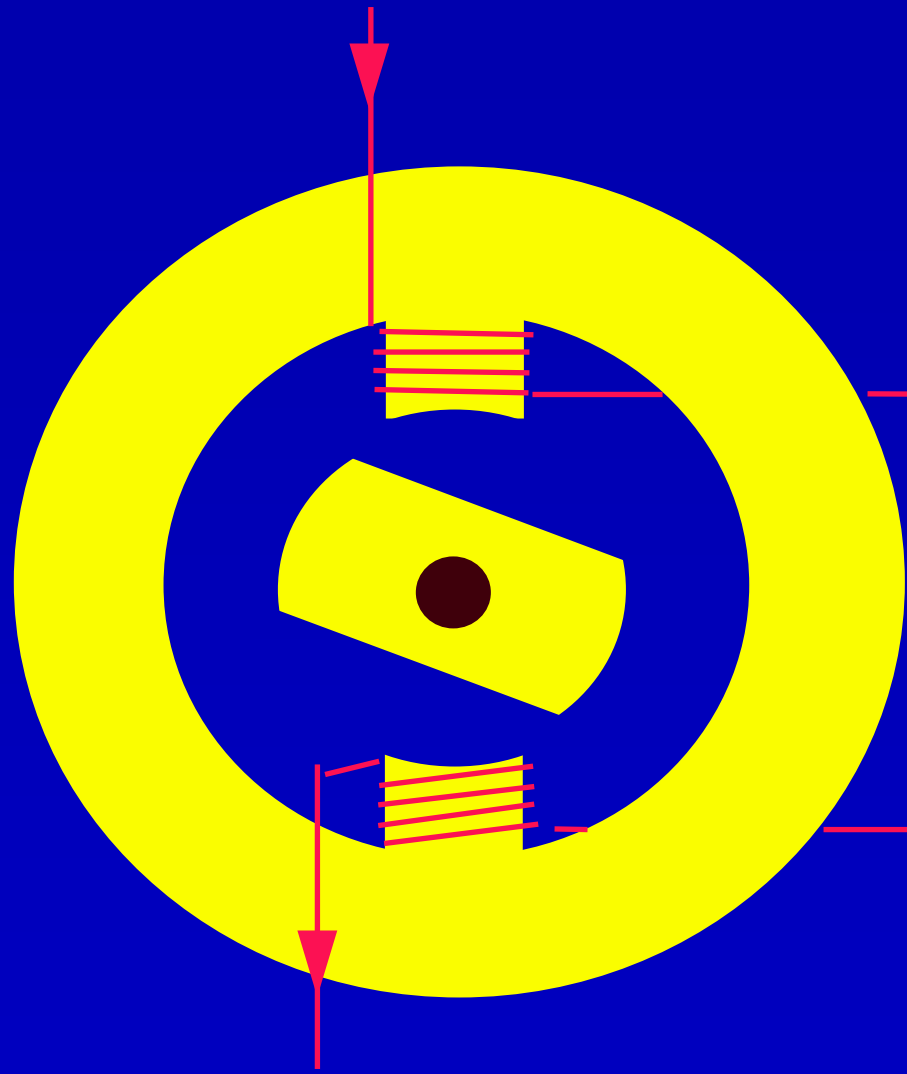
No
torque



Phase
current
ON


CW
rotation

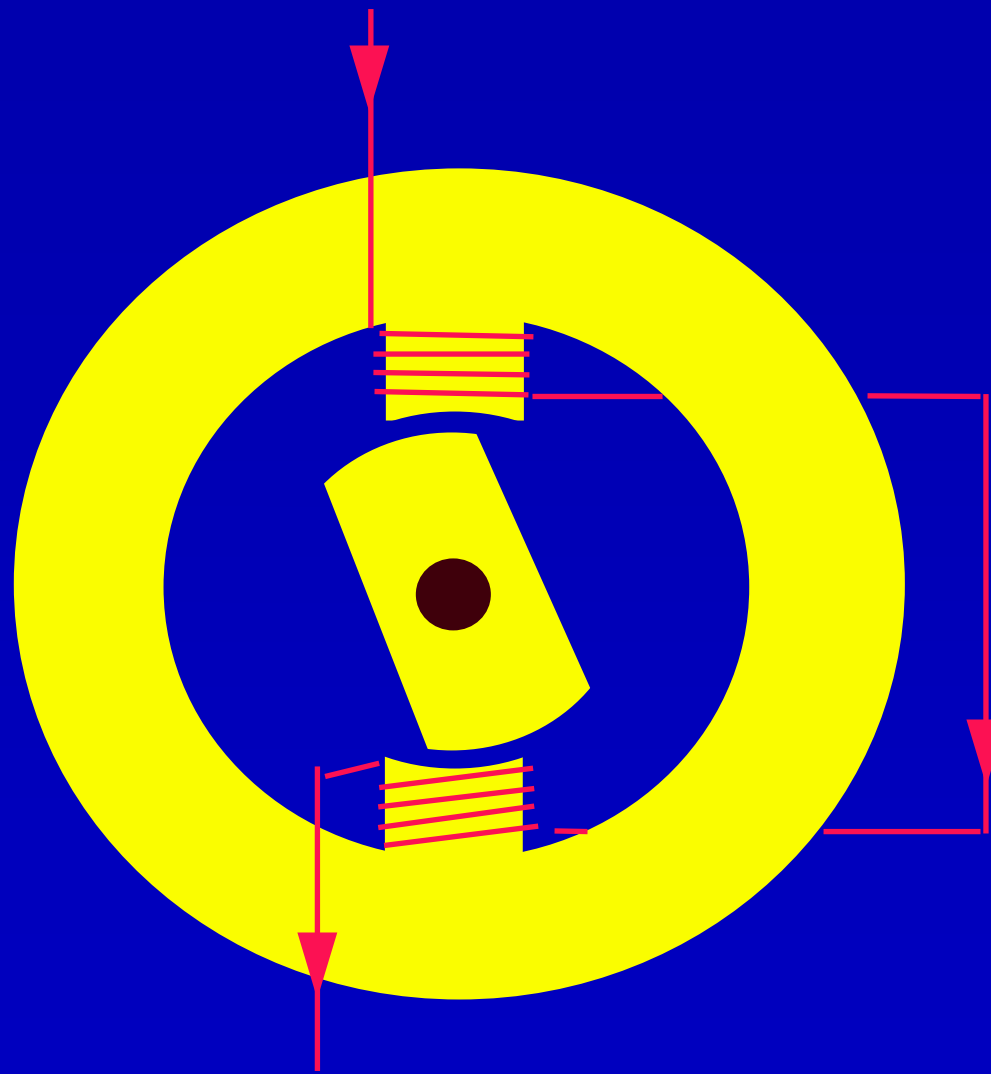

CW
torque



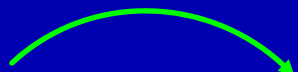
Phase
current
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CW
rotation

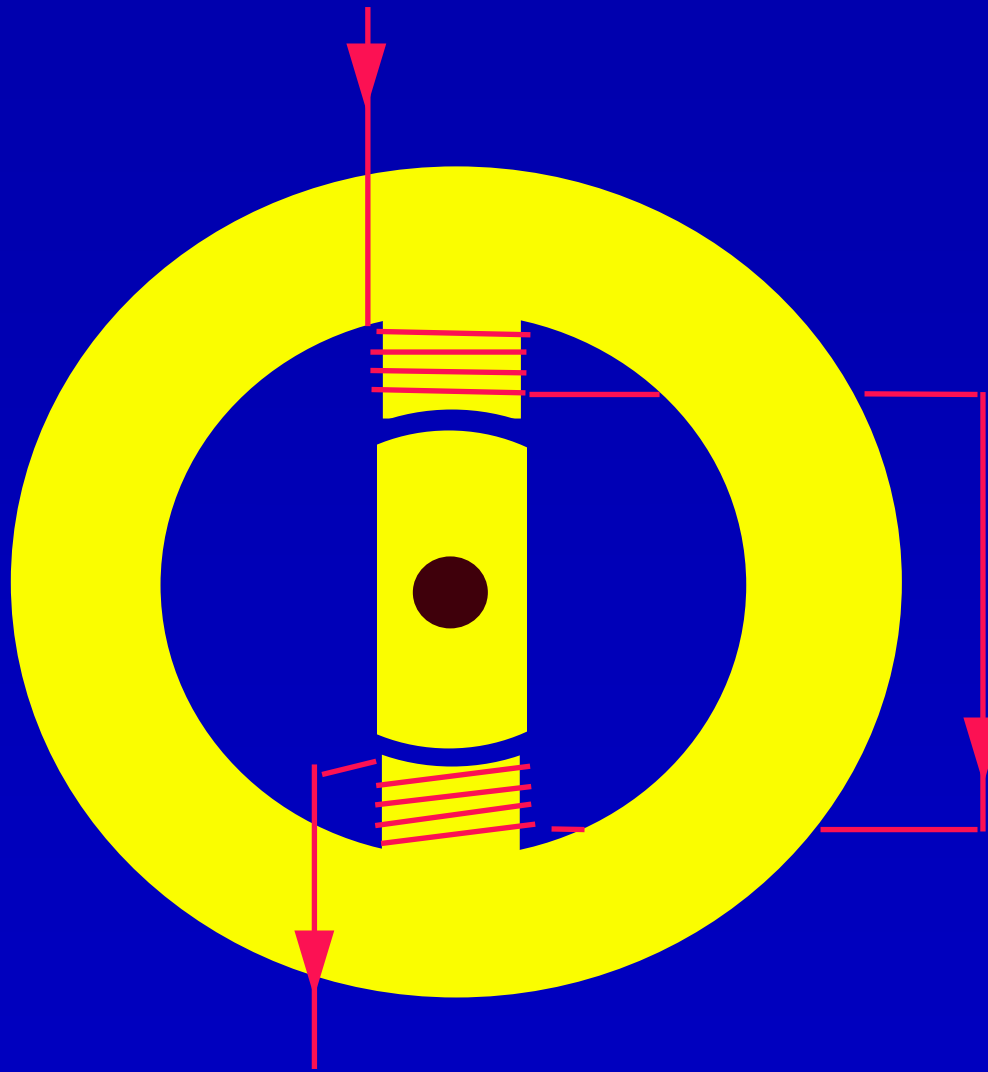
CW
torque



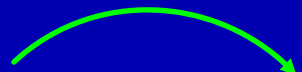
Phase
current
ON


CW
rotation

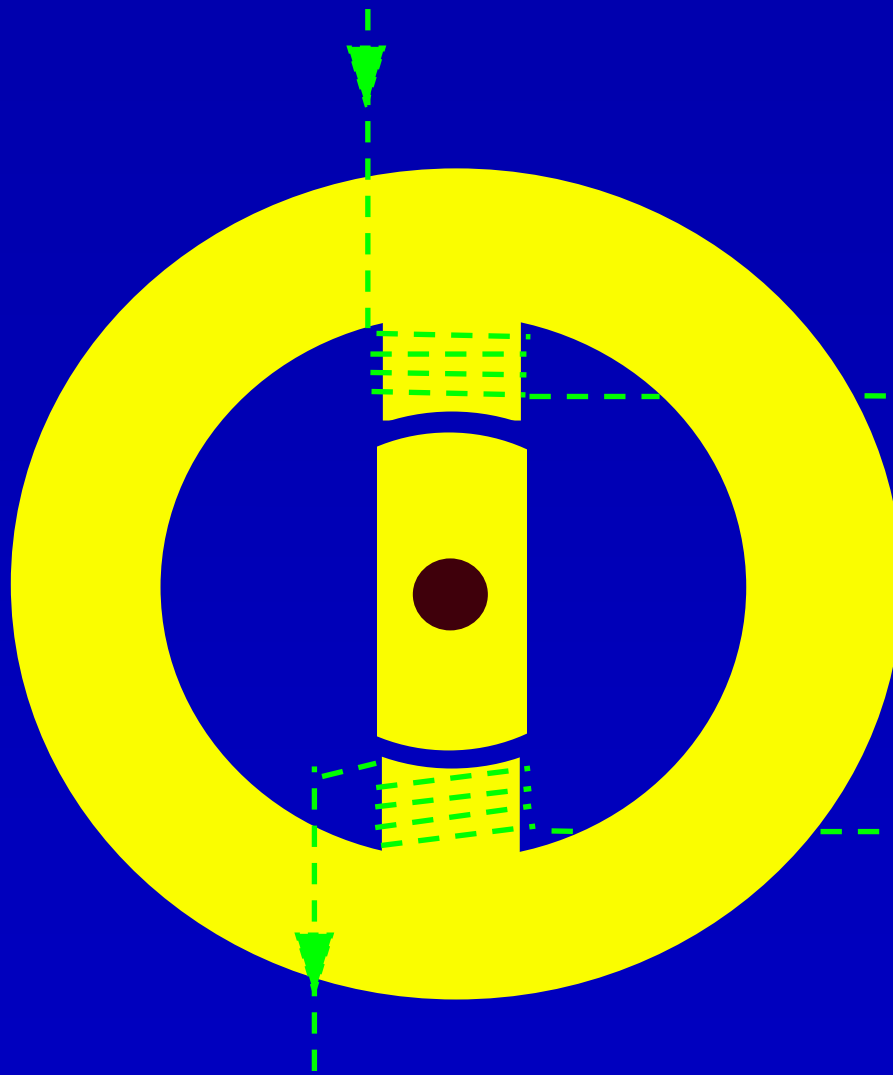
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torque



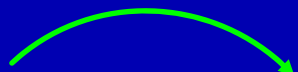
Phase
current
ON


CW
rotation

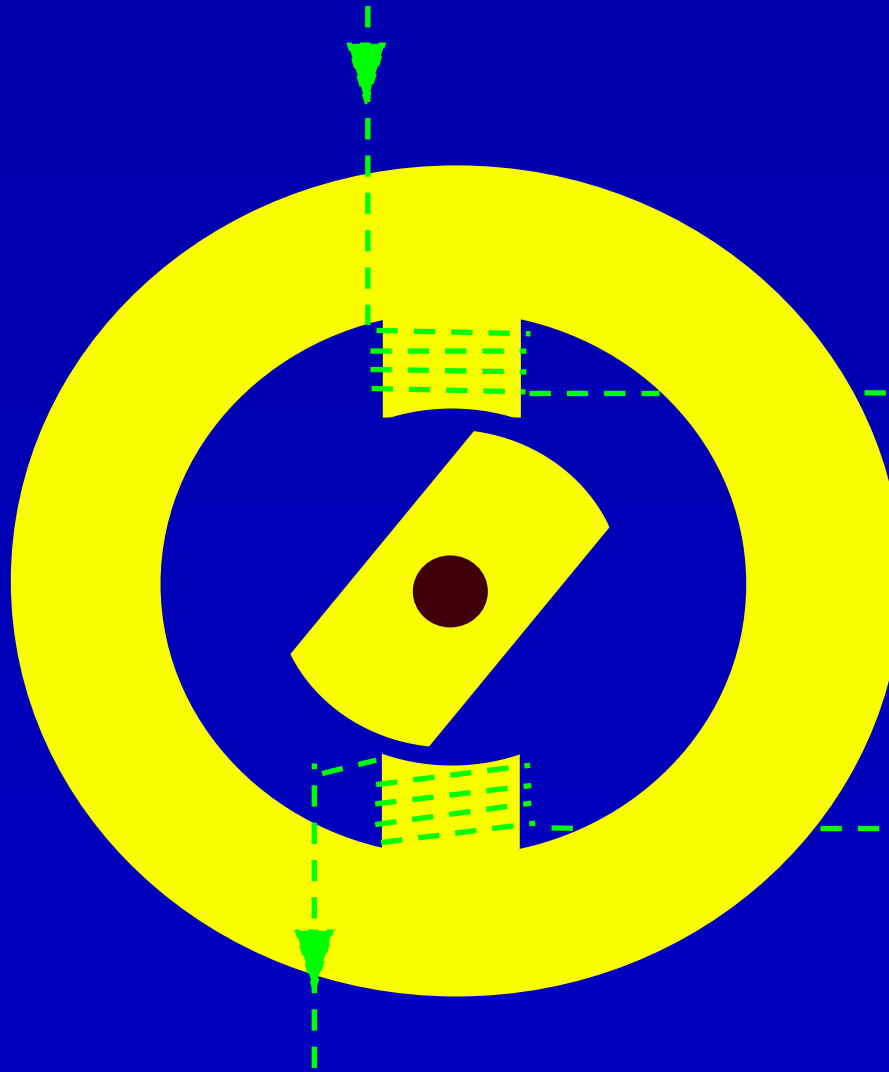
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torque



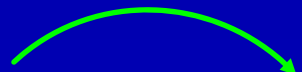
Phase
current
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CW
rotation

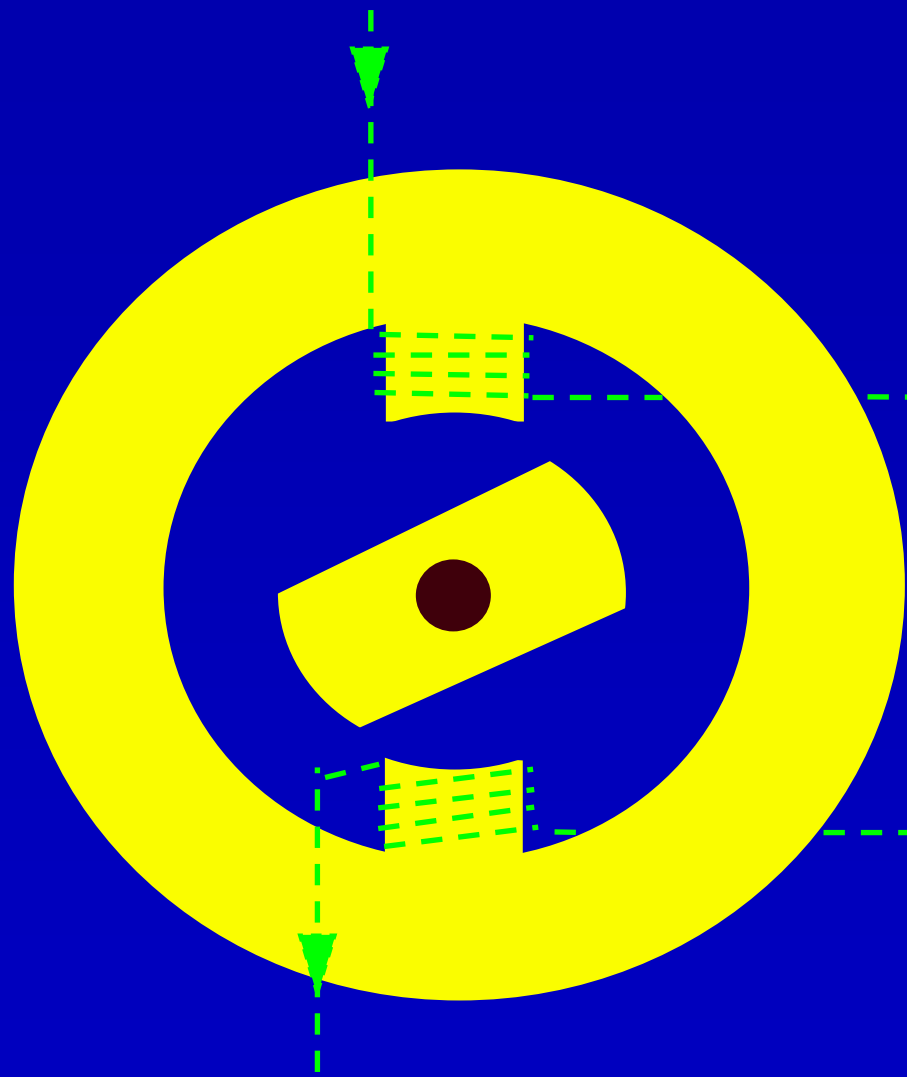
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torque



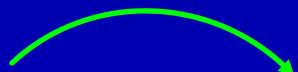
Phase
current
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CW
rotation

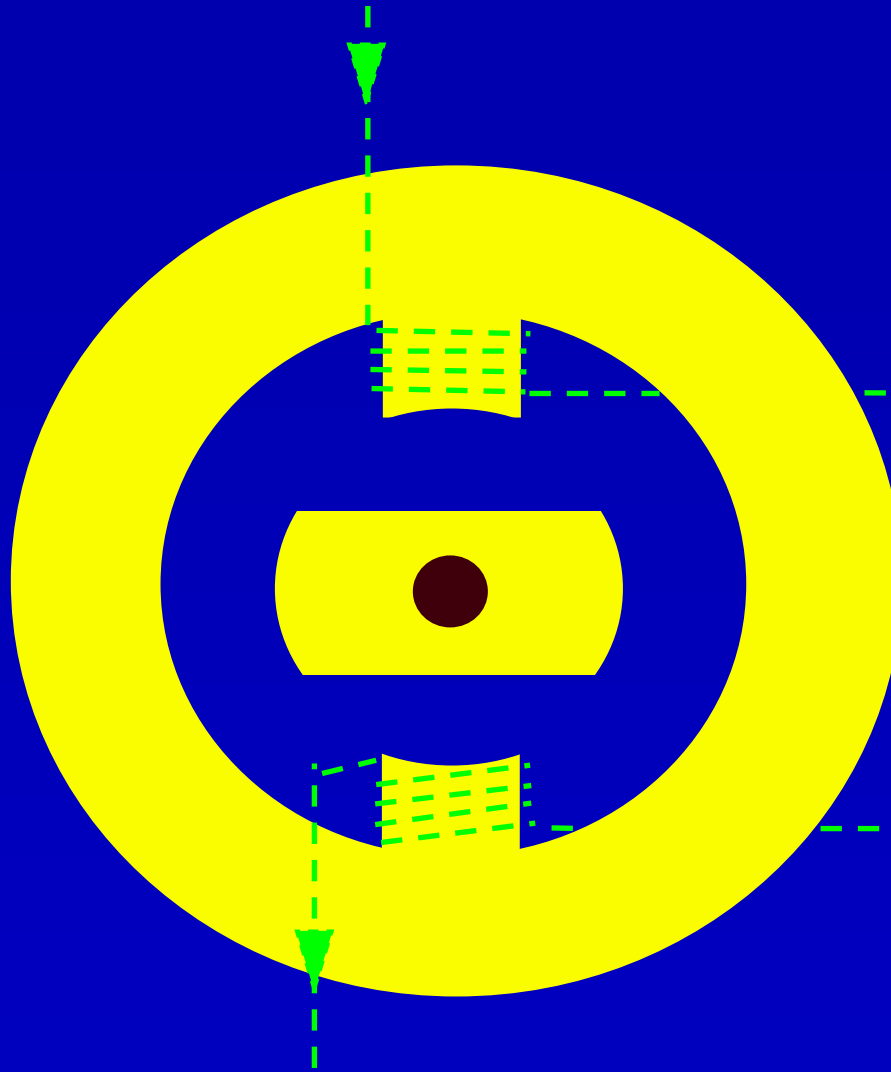
No
torque



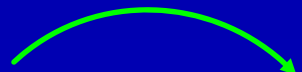
Phase
current
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CW
rotation

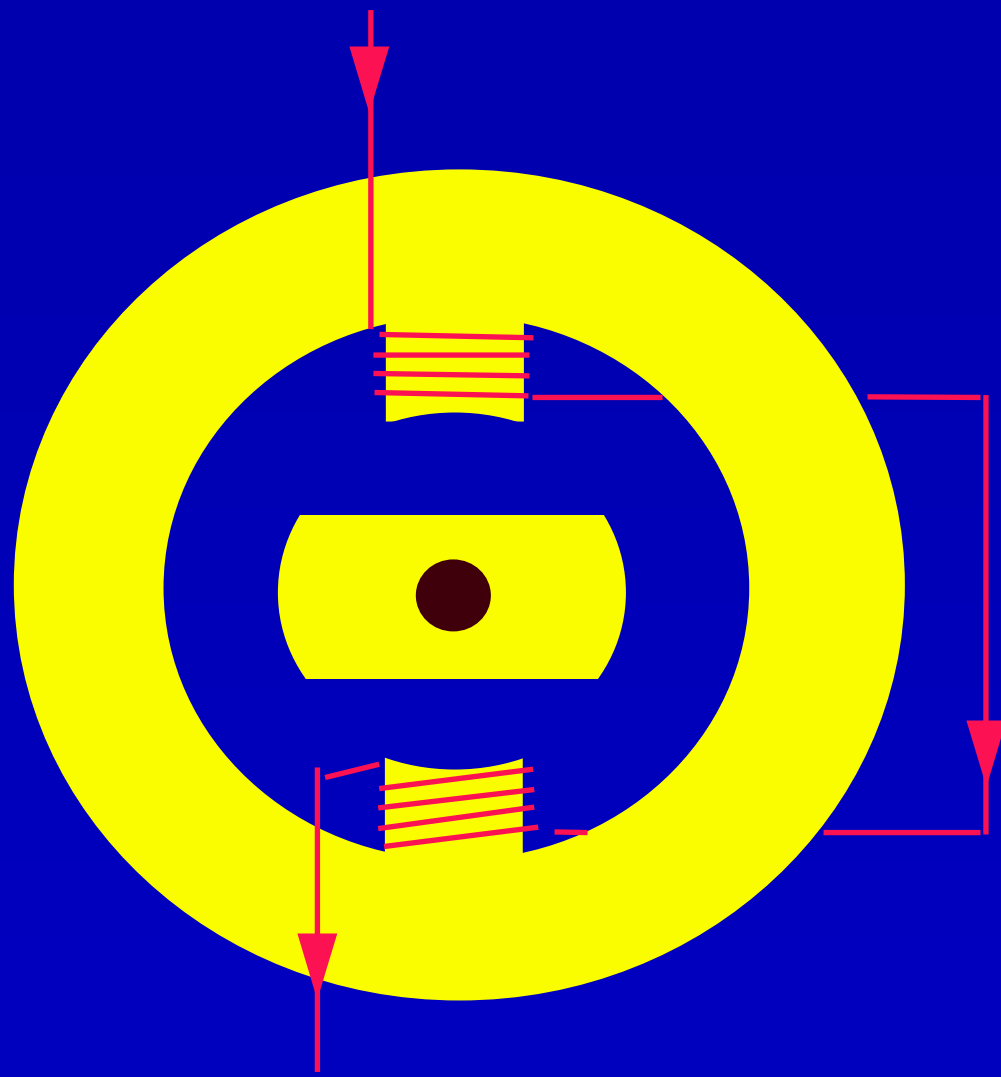
No
torque



Phase
current
= ZERO


CW
rotation

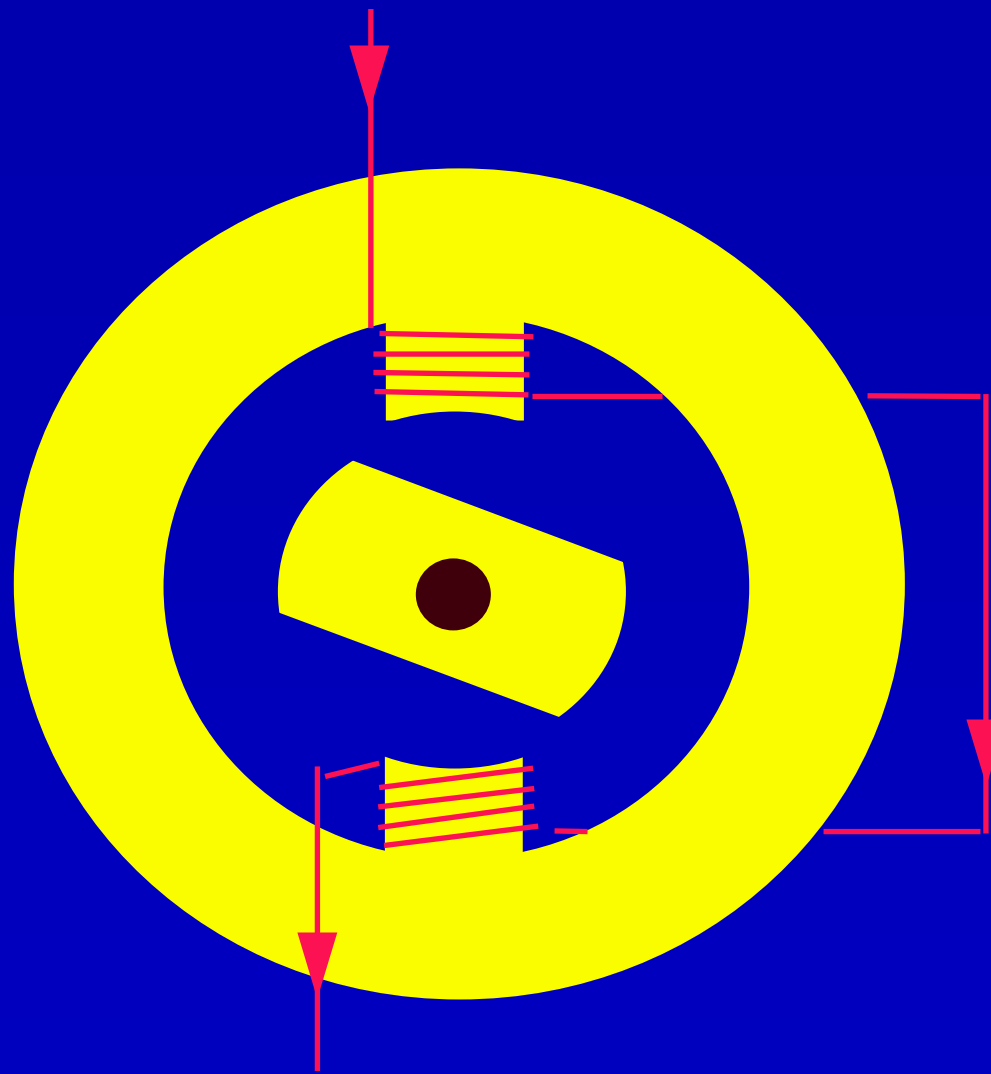
No
torque



Phase
current
ON

CW
rotation

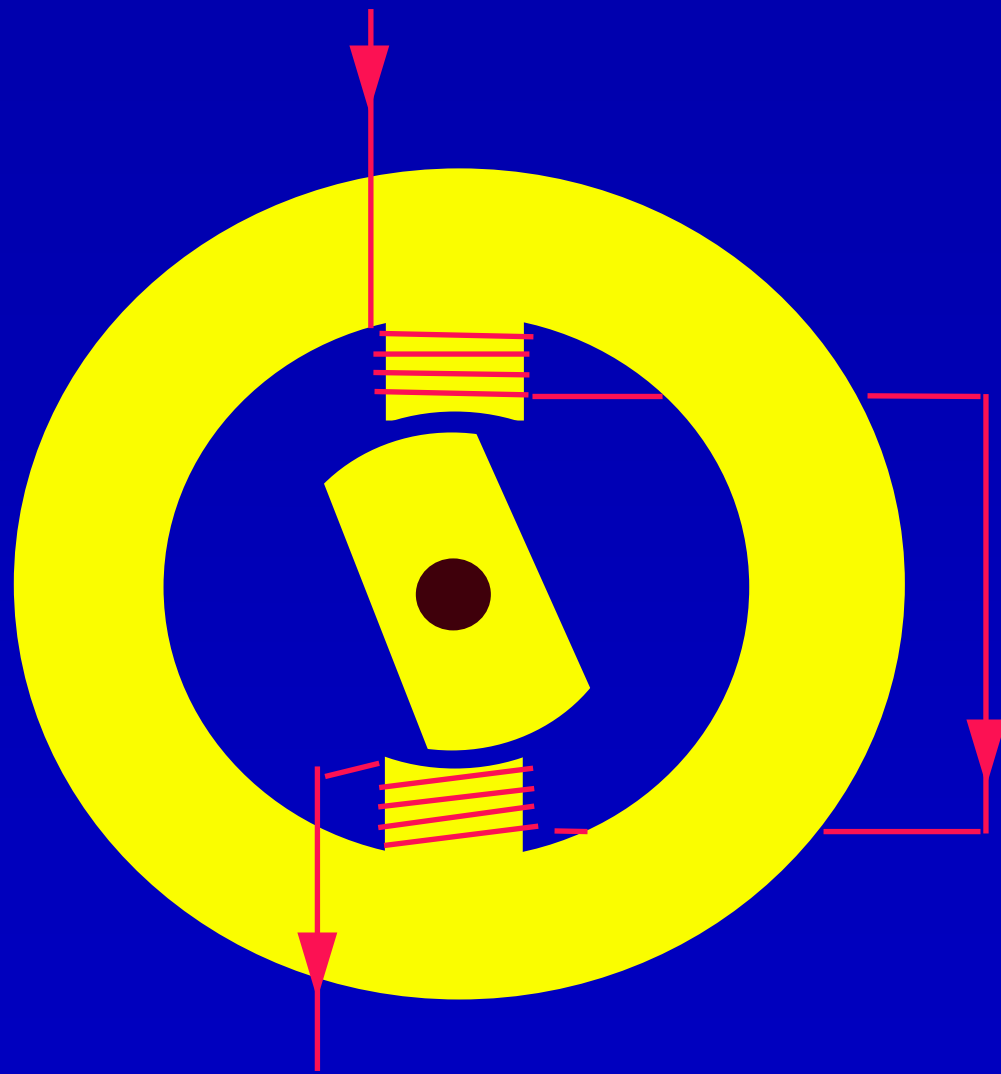
CW
torque



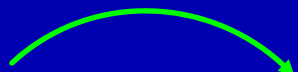
Phase
current
ON

CW
rotation

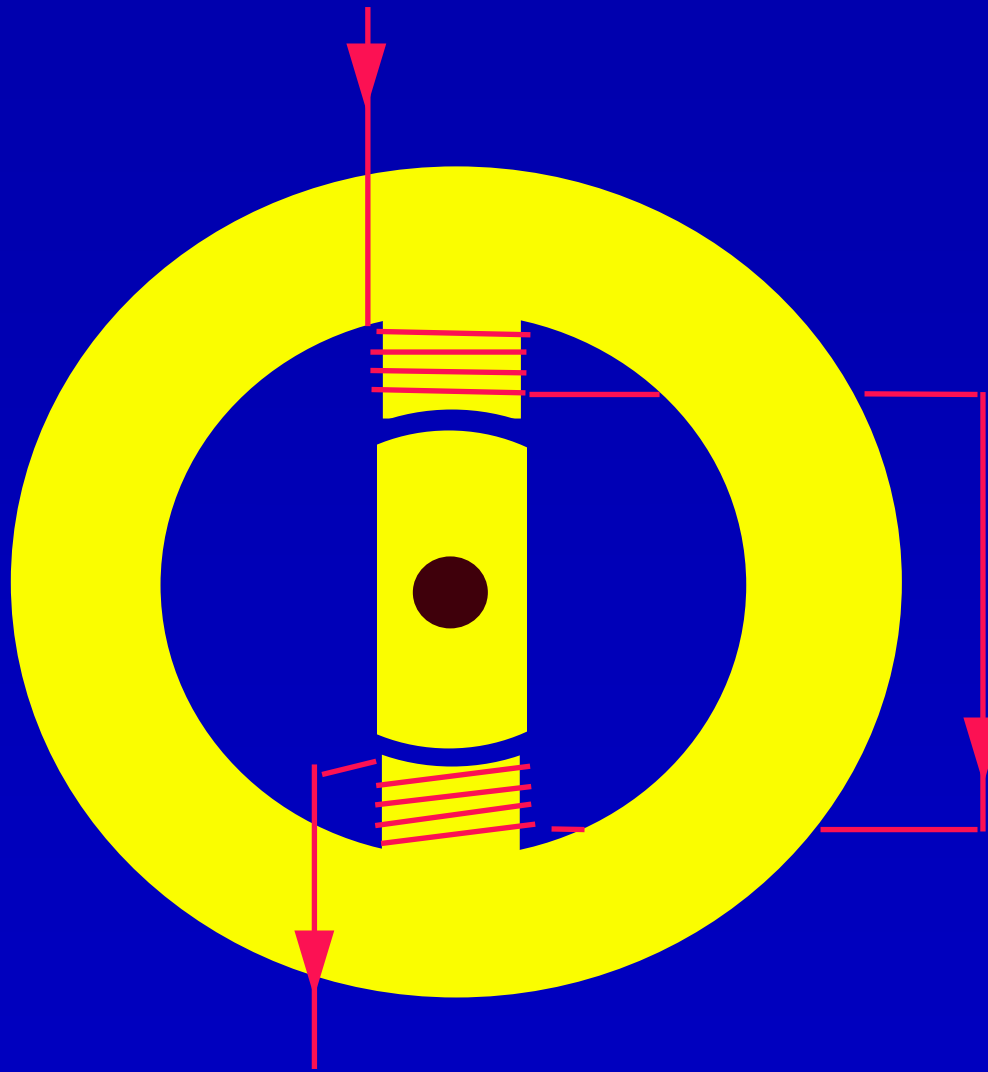
CW
torque



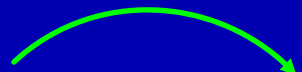
Phase
current
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CW
rotation

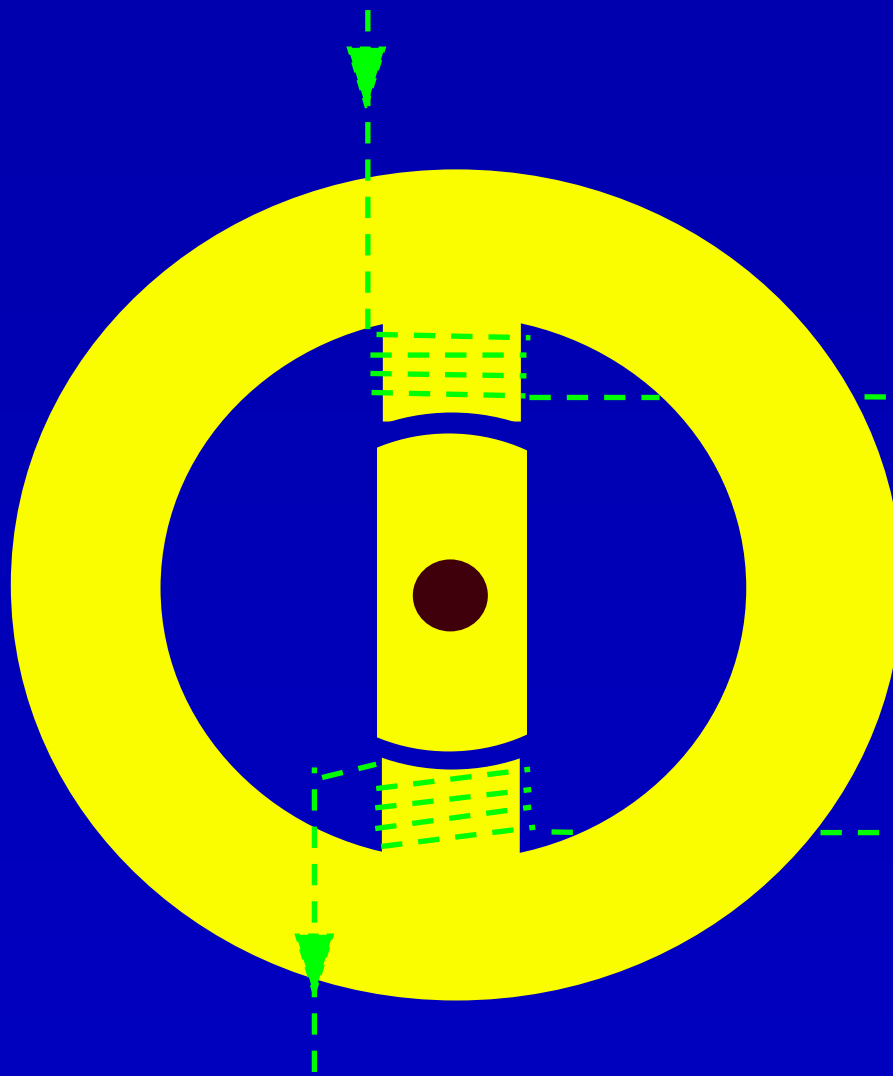
No
torque



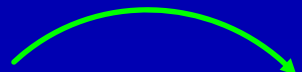
Phase
current
ON


CW
rotation

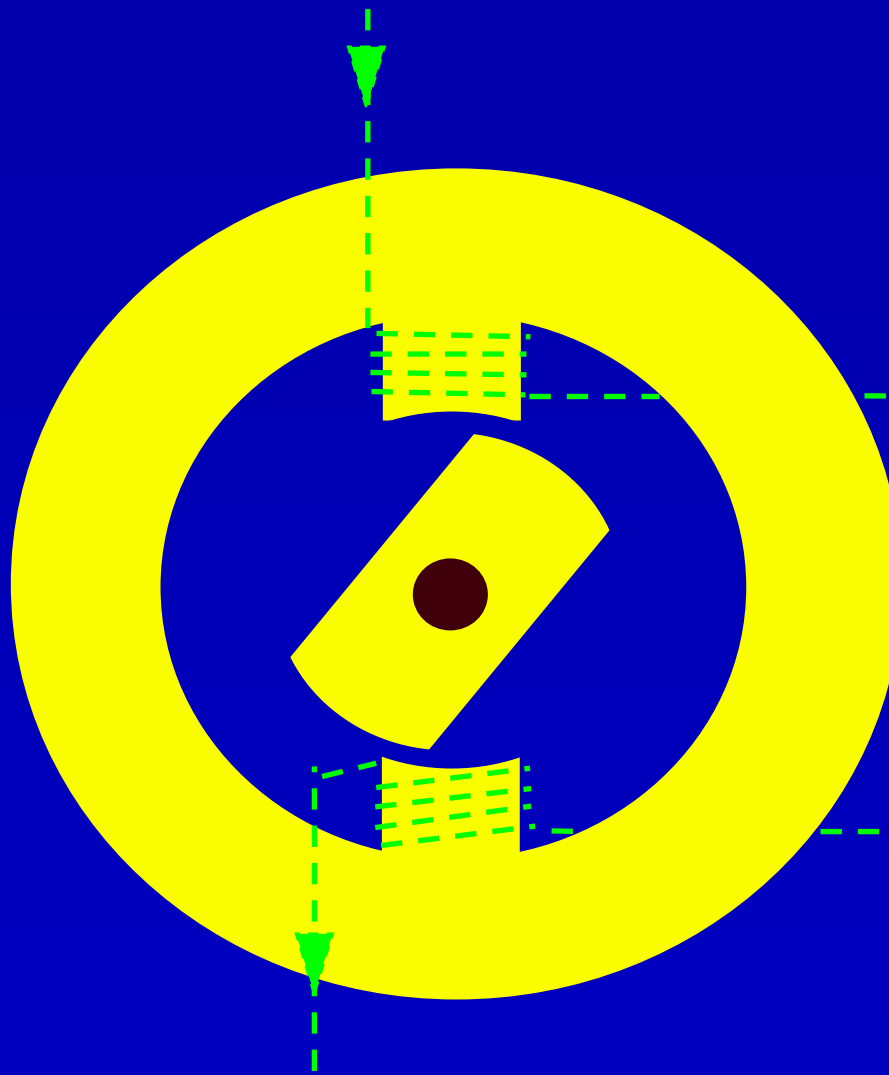
No
torque



Phase
current
= ZERO


CW
rotation

No
torque



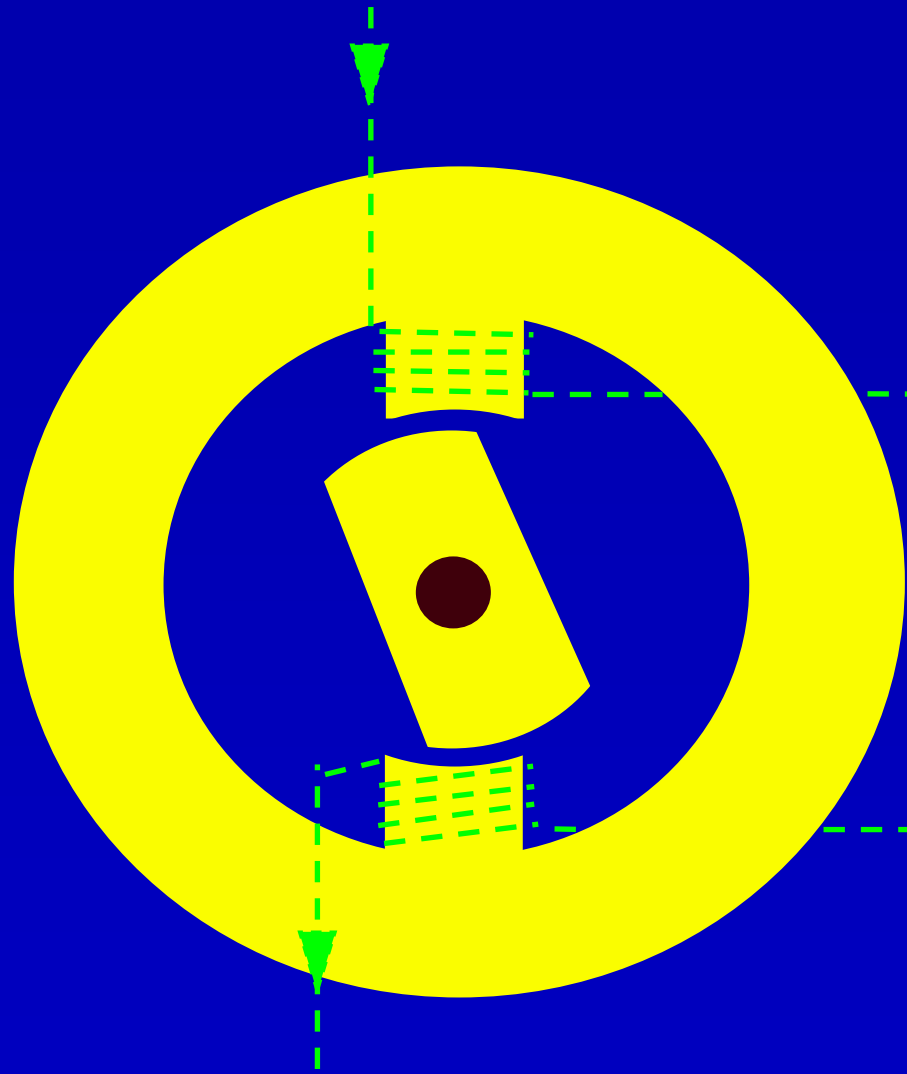
Phase
current
= ZERO

Operation as a brake or electrical generator

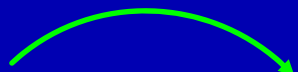
- Exact dual of motoring operation
- Braking torque is produced when rotor & stator poles are being “pulled apart” – i.e. when inductance is falling
- Switch phase current (and magnetic flux) ON at TDC (*ideally*)
- Switch phase current (and magnetic flux) OFF at BDC (*ideally*)


CW
rotation

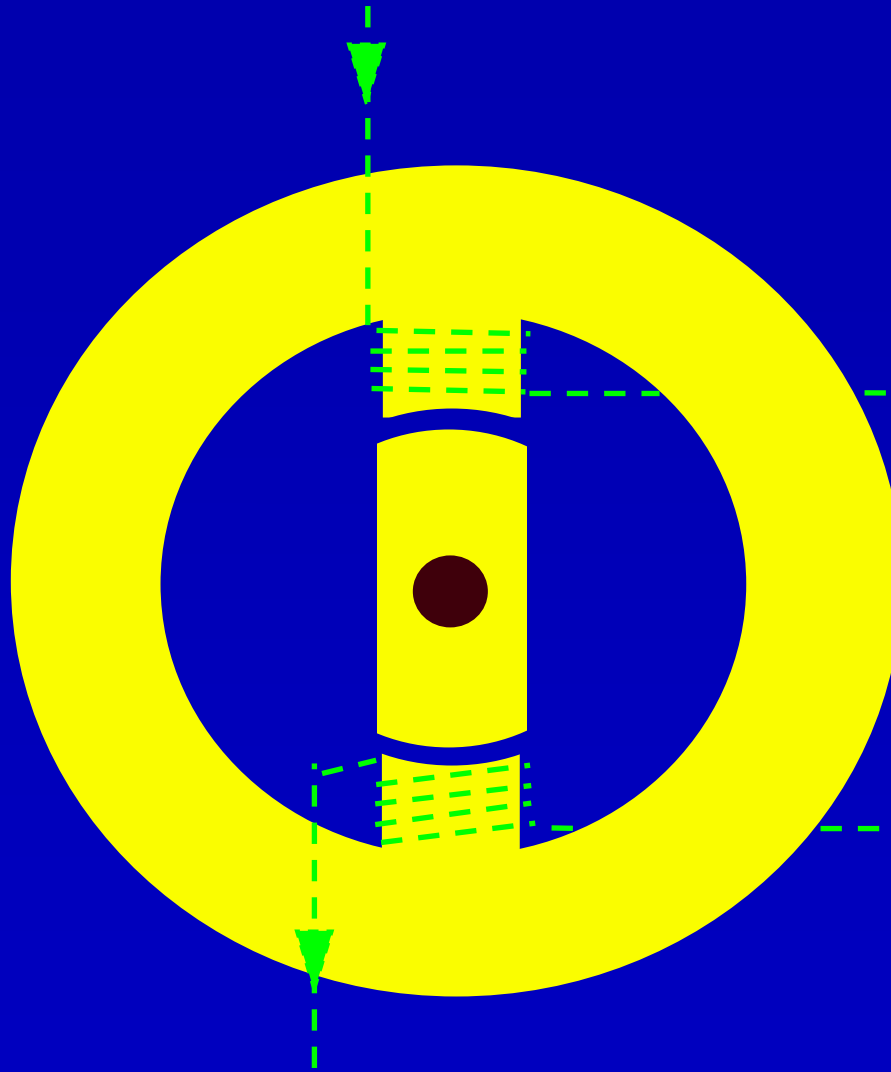
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torque



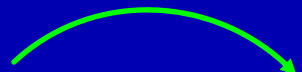
Phase
current
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CW
rotation

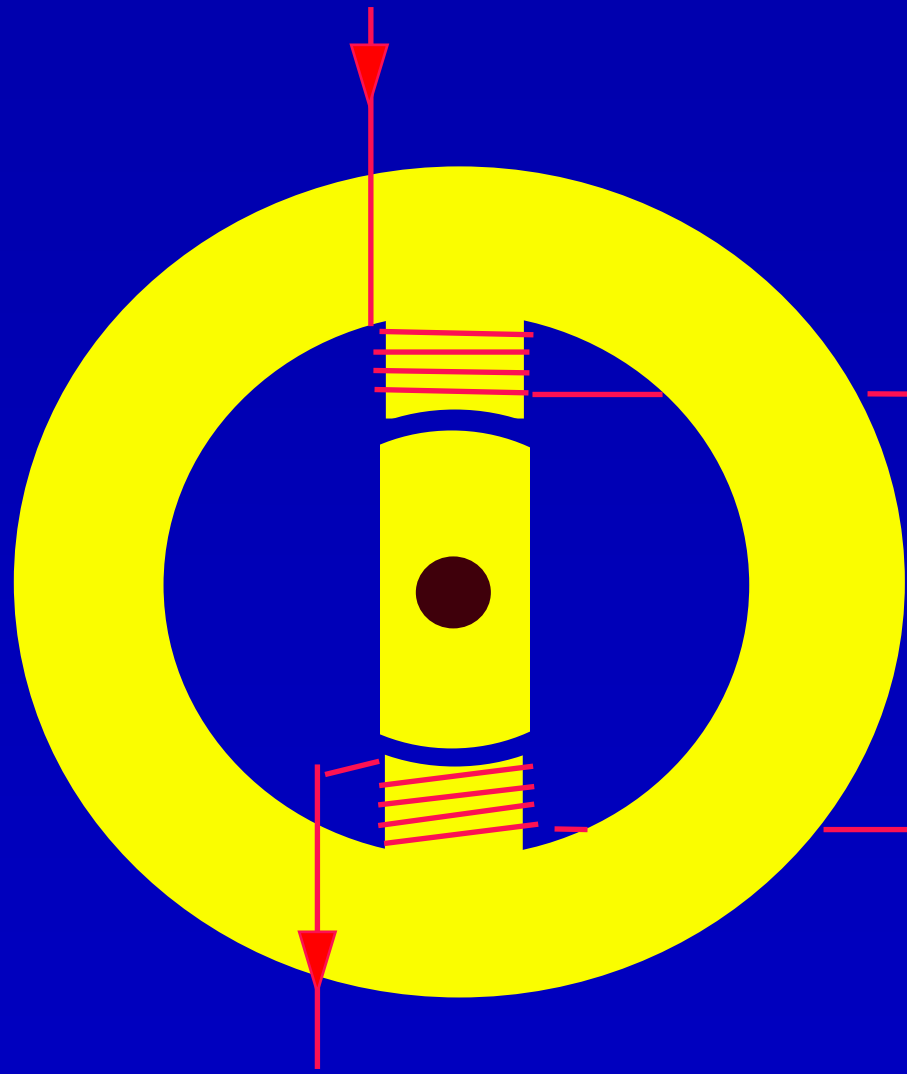
No
torque



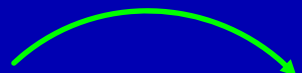
Phase
current
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CW
rotation

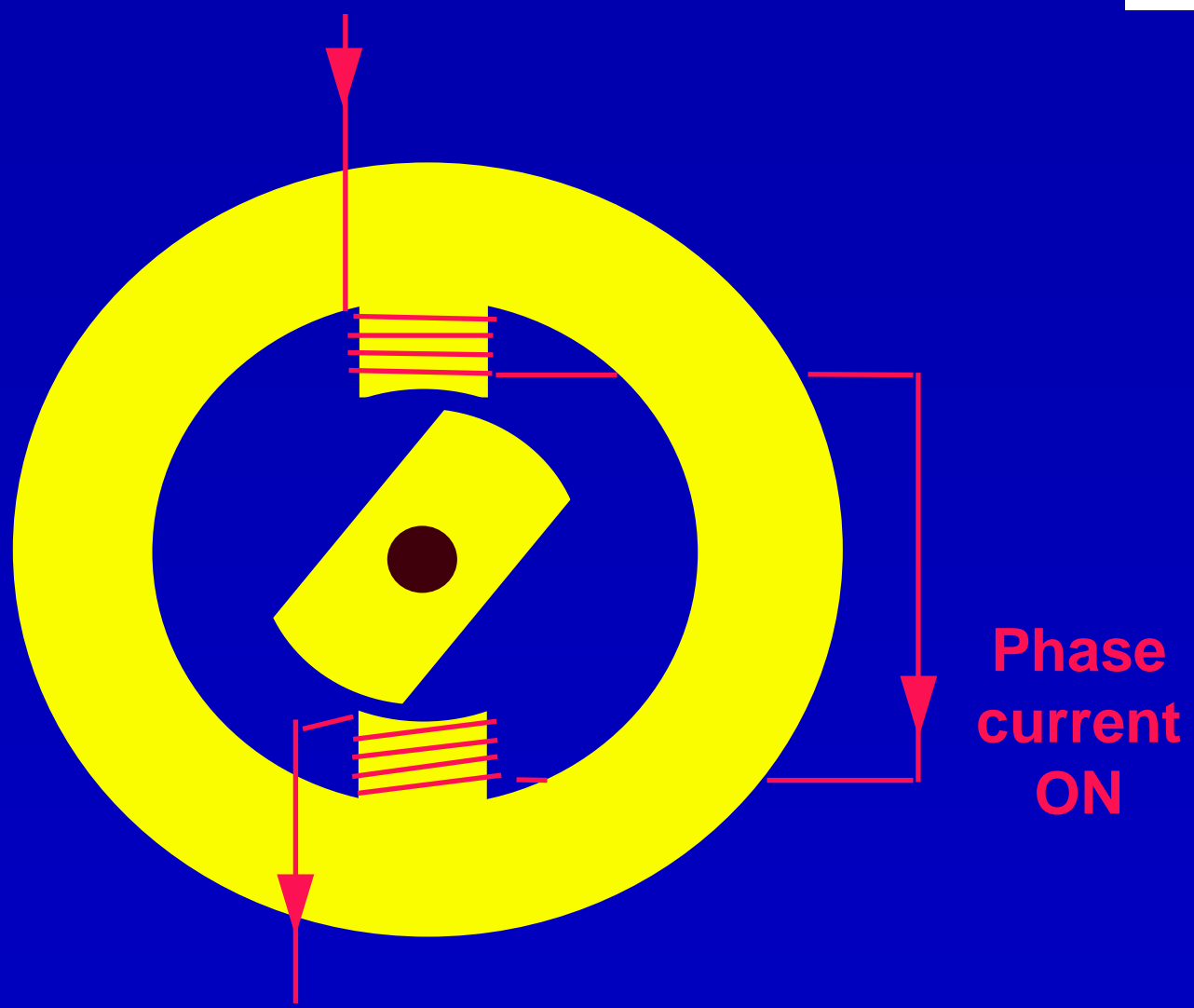
No
torque

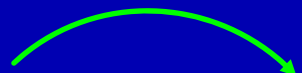


Phase
current
ON

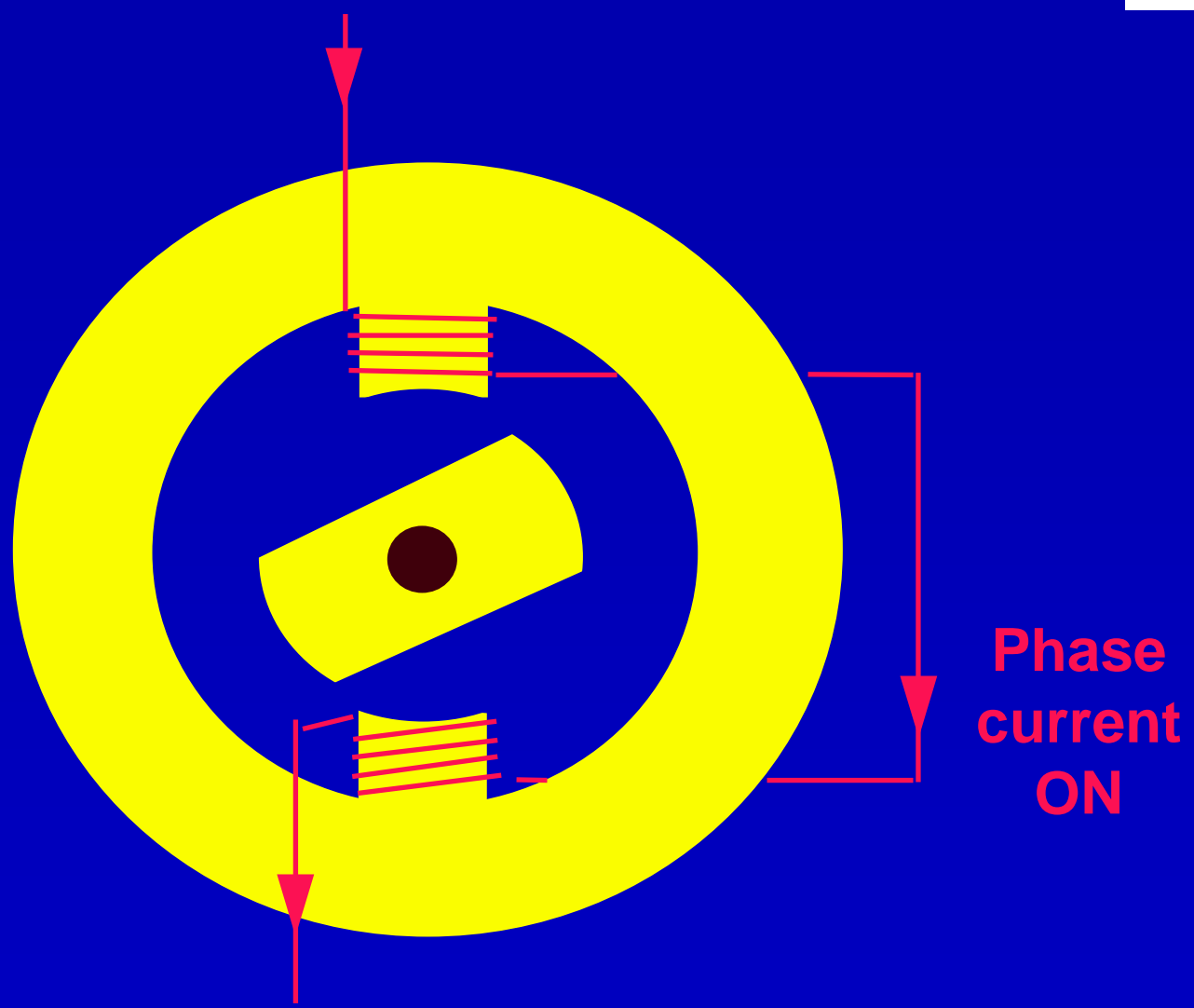

CW
rotation

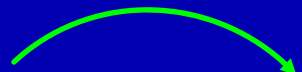

CCW
torque



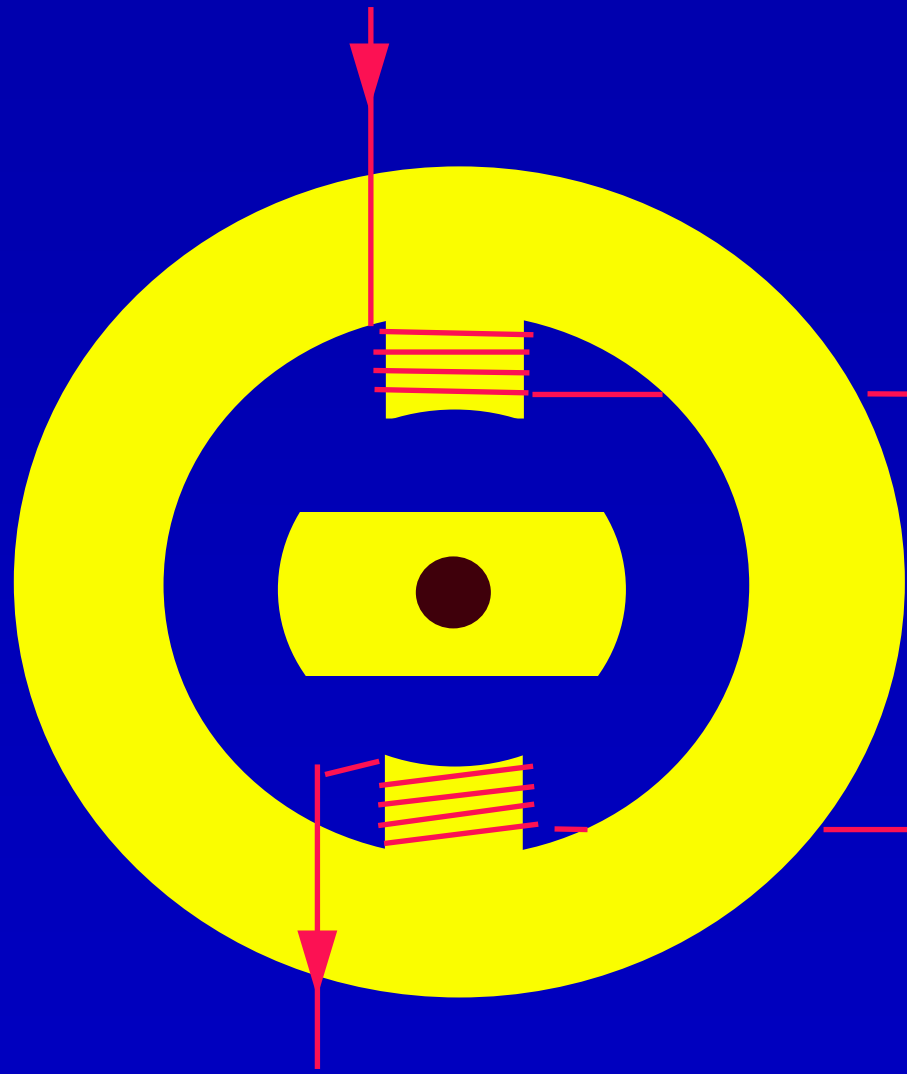

CW
rotation


CCW
torque

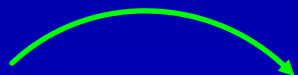



CW
rotation

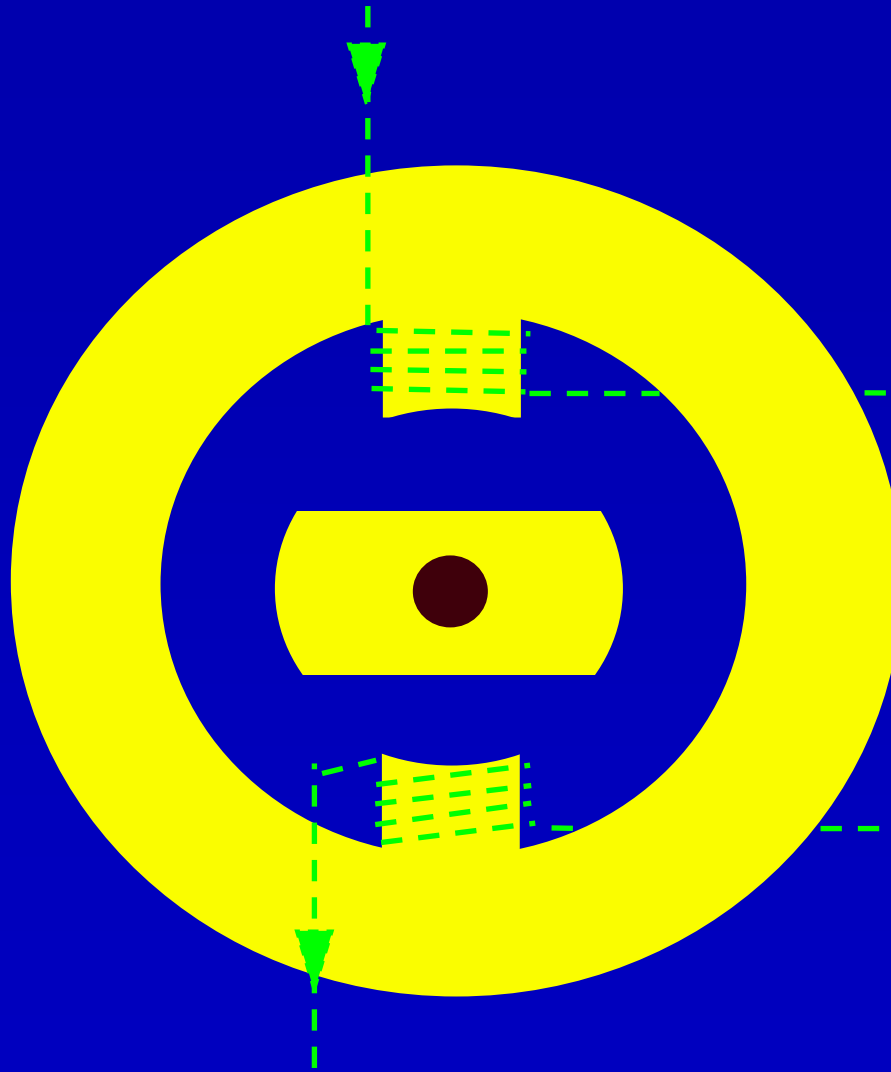
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torque



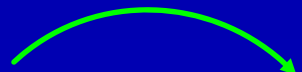
Phase
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CW
rotation

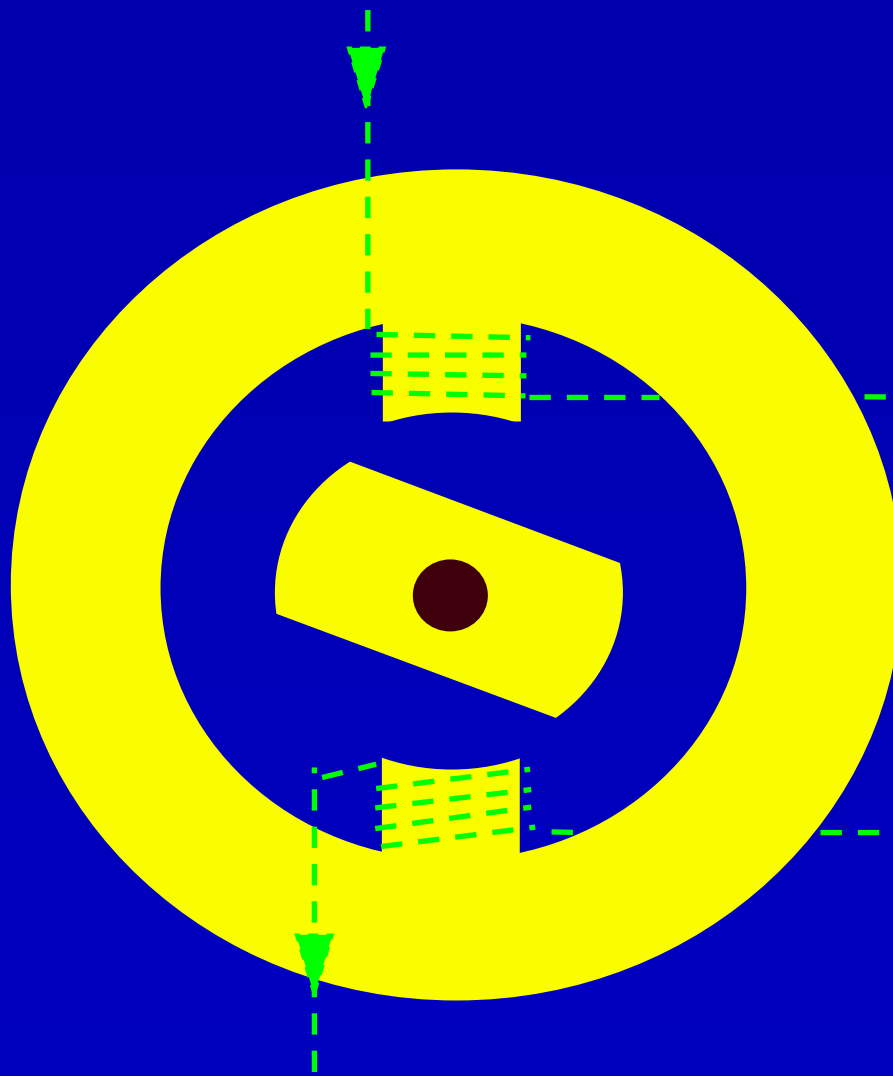
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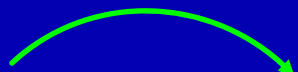
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CW
rotation

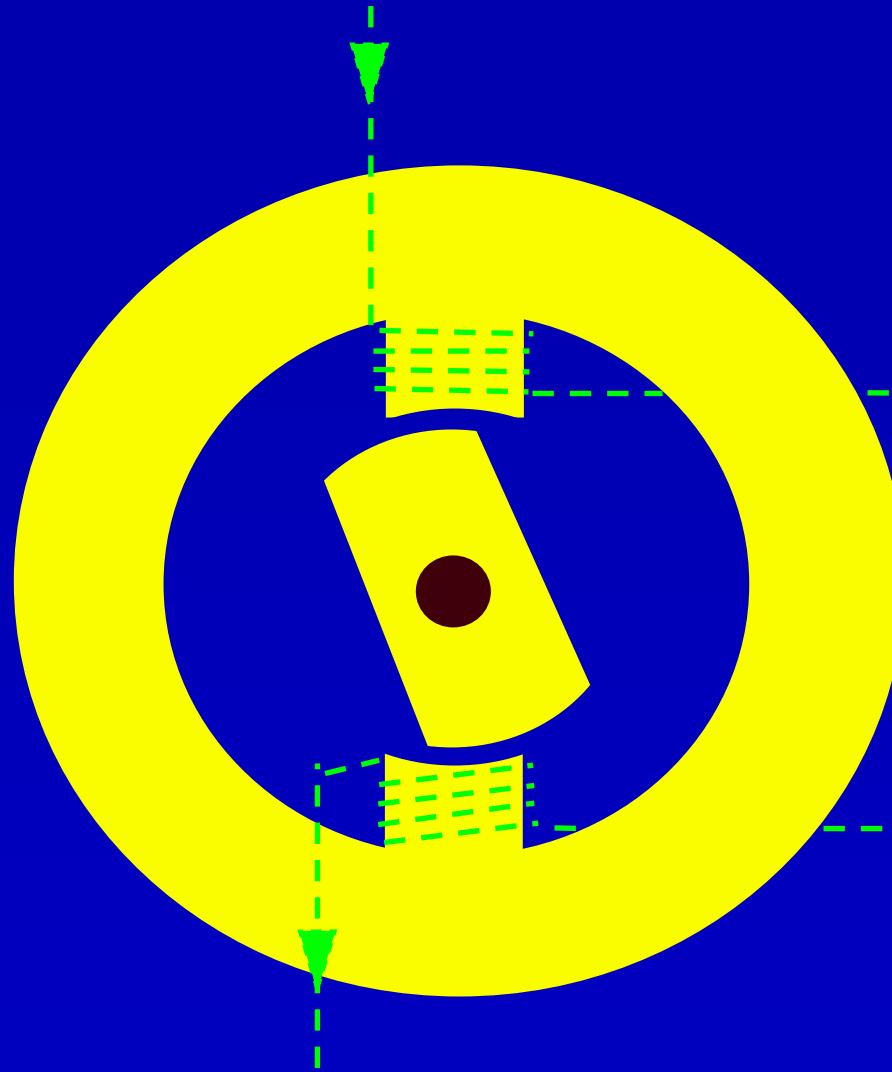
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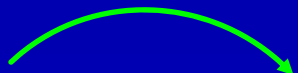
Phase
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CW
rotation

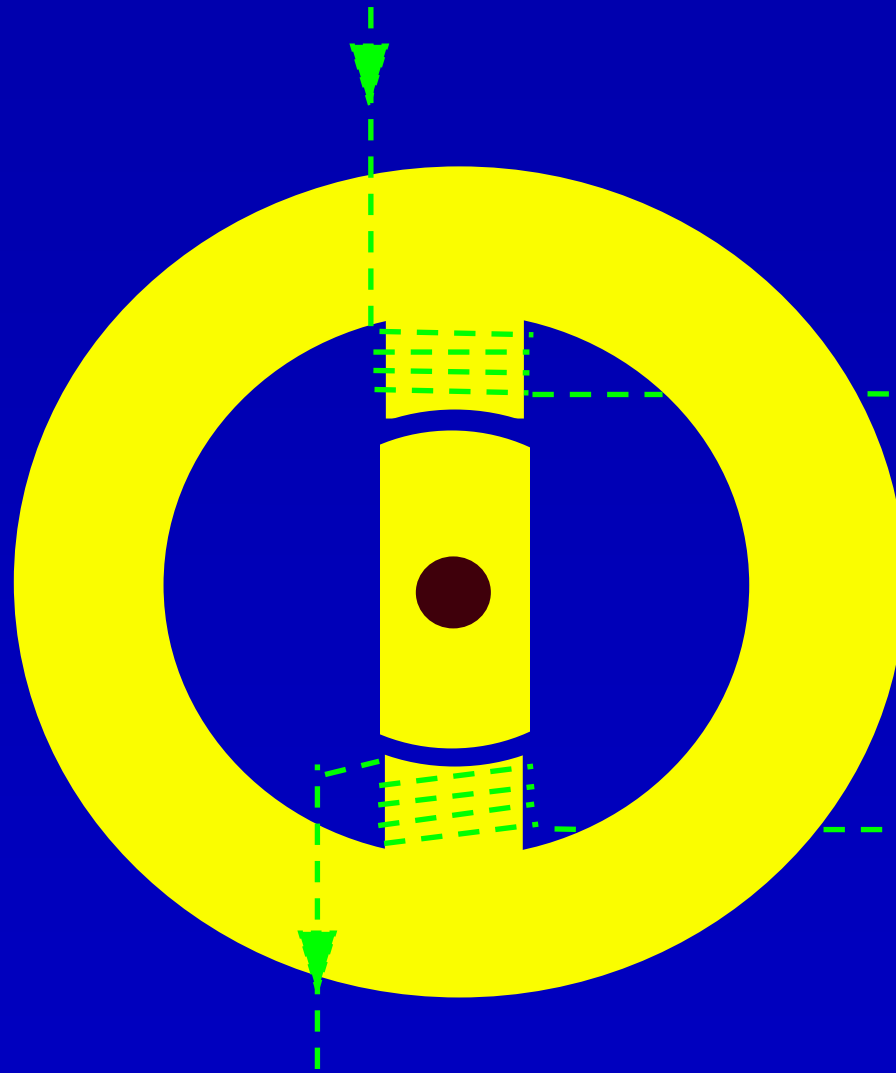
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torque



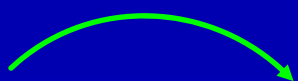
Phase
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CW
rotation

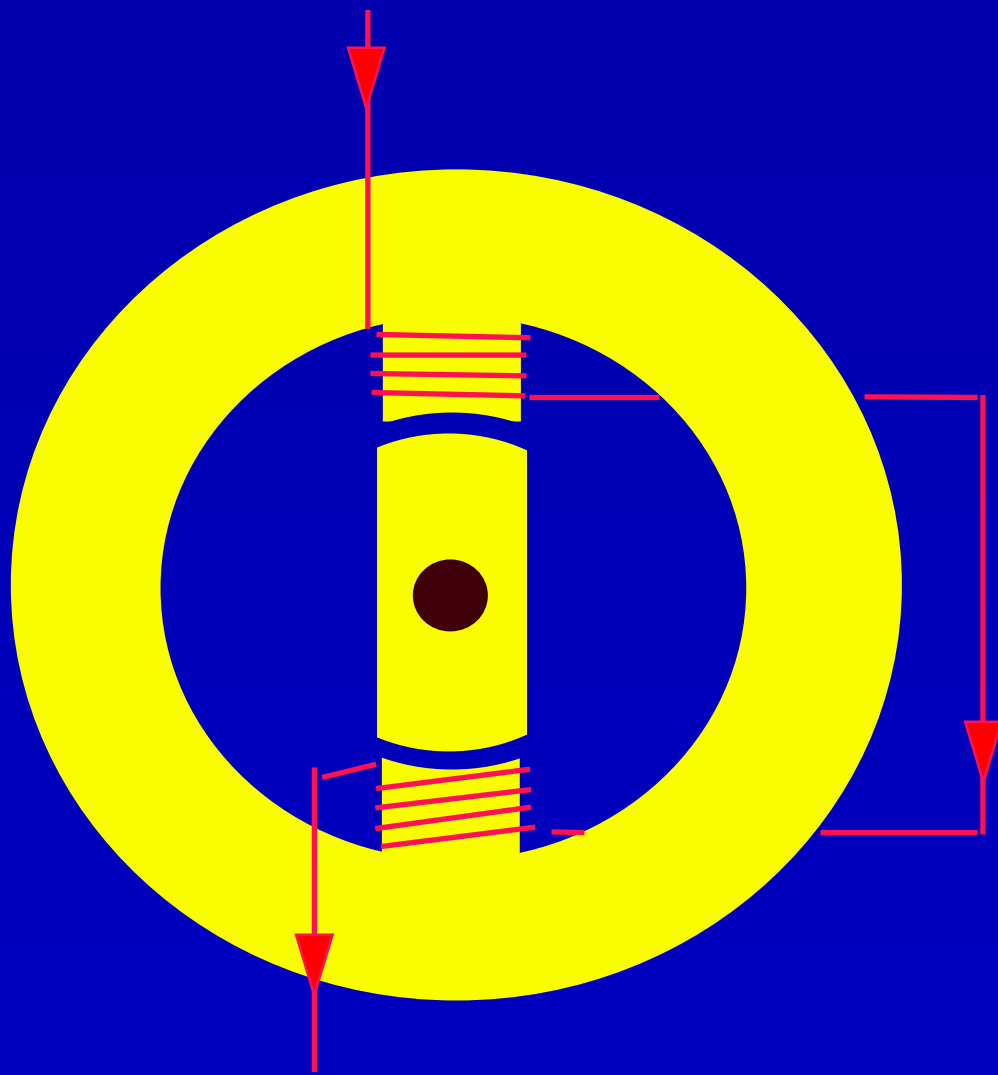
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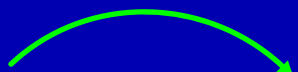
Phase
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CW
rotation

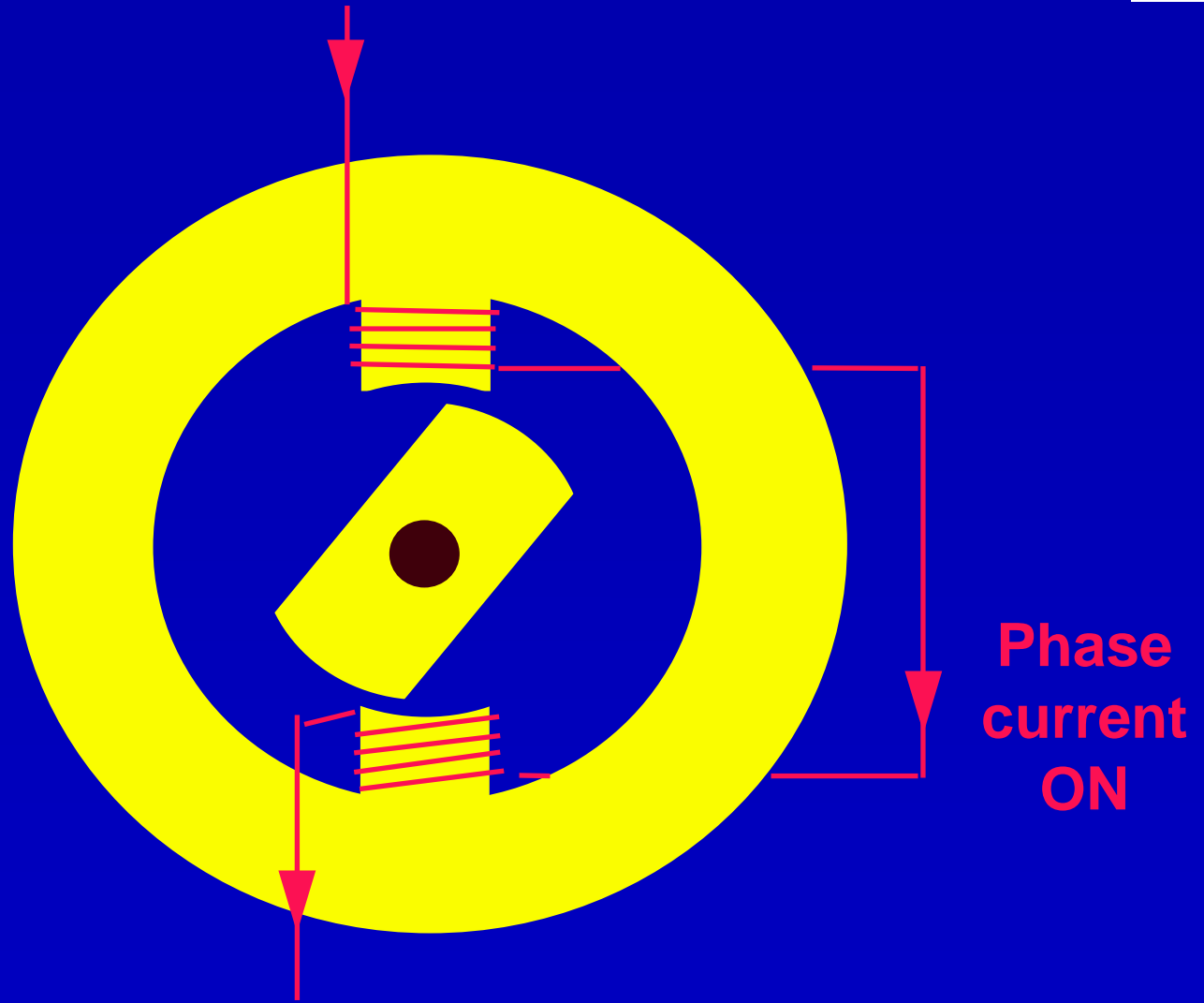
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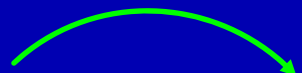


Phase
current
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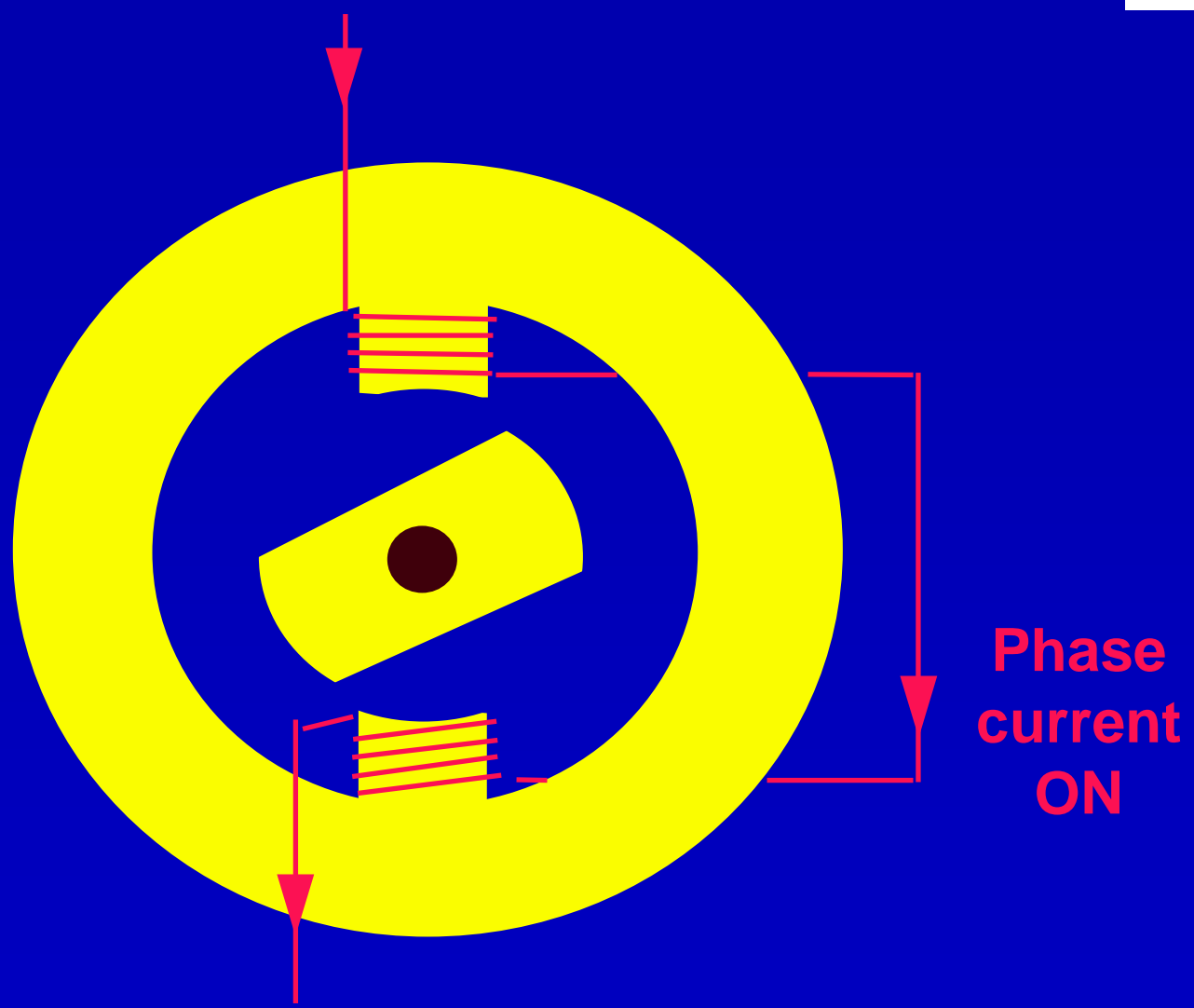

CW
rotation

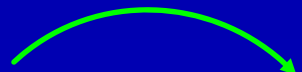

CCW
torque



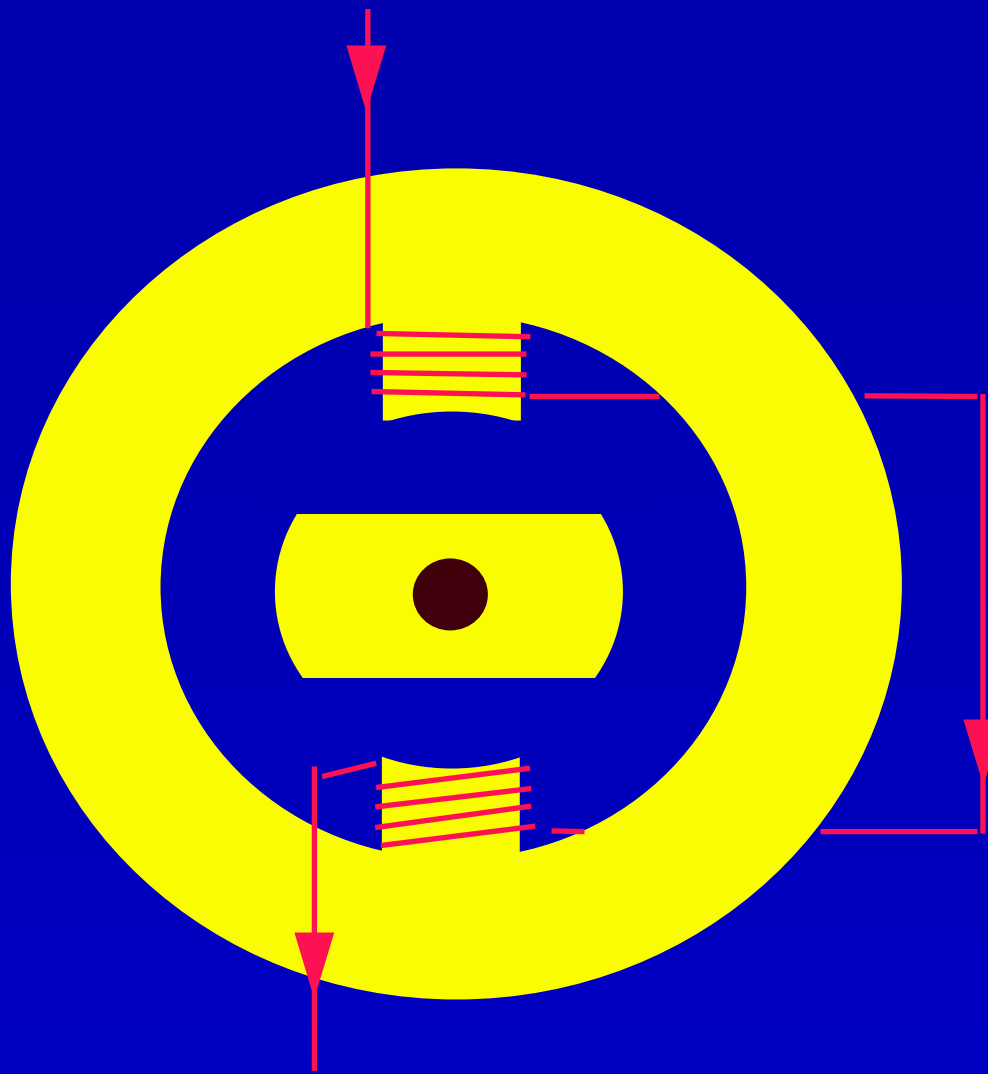

CW
rotation


CCW
torque

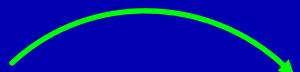



CW
rotation

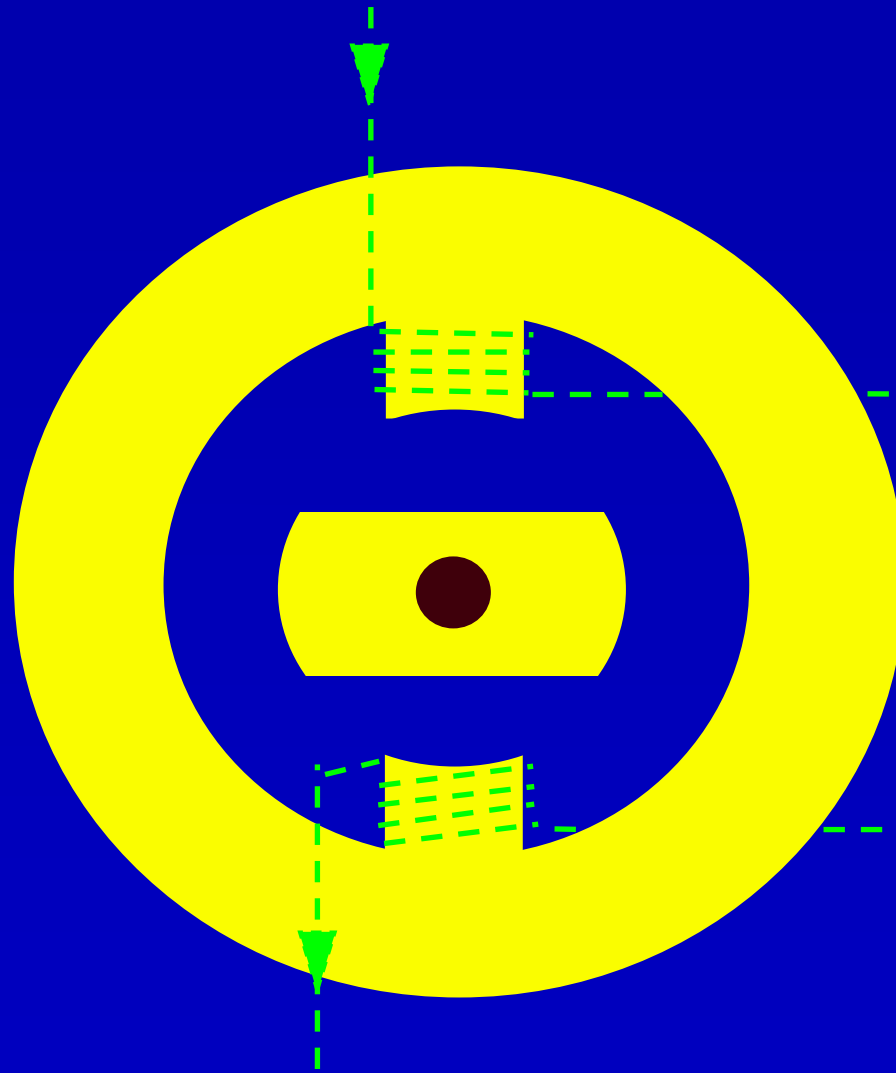
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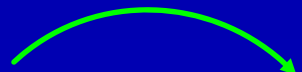
Phase
current
ON


CW
rotation

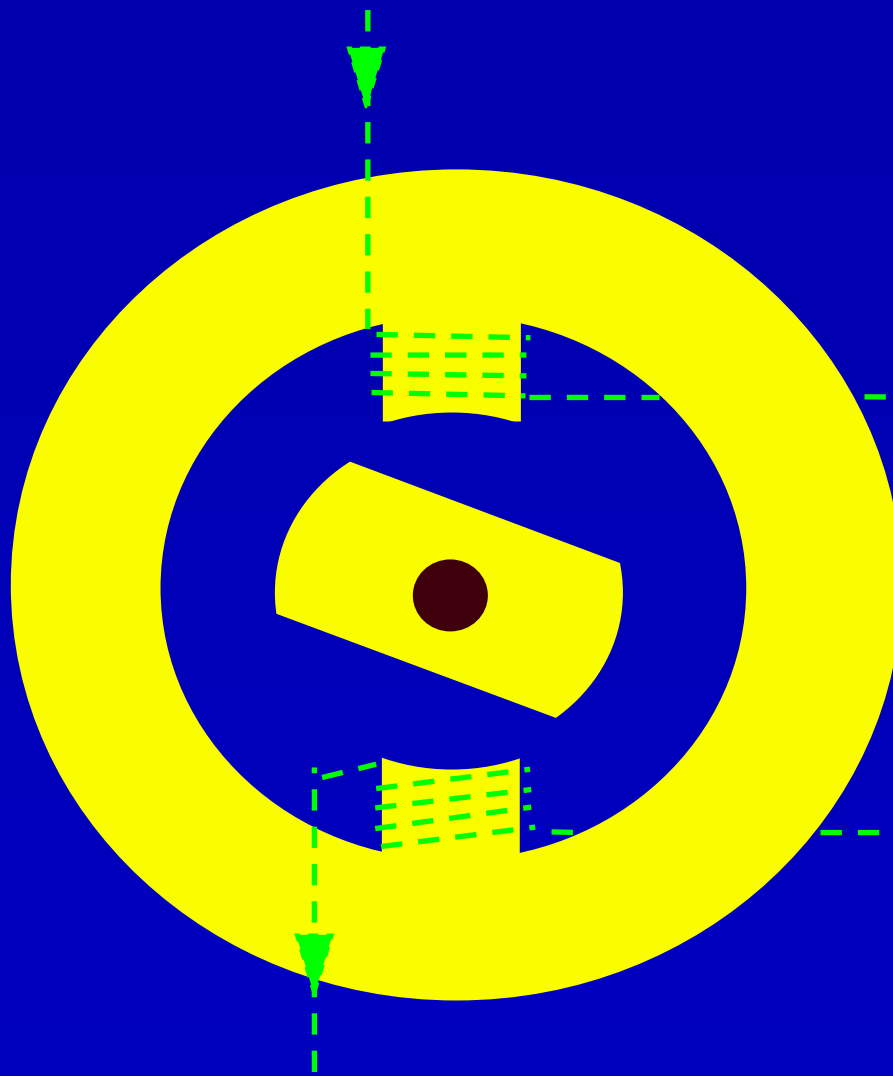
No
torque



Phase
current
= ZERO


CW
rotation

No
torque



Phase
current
= ZERO

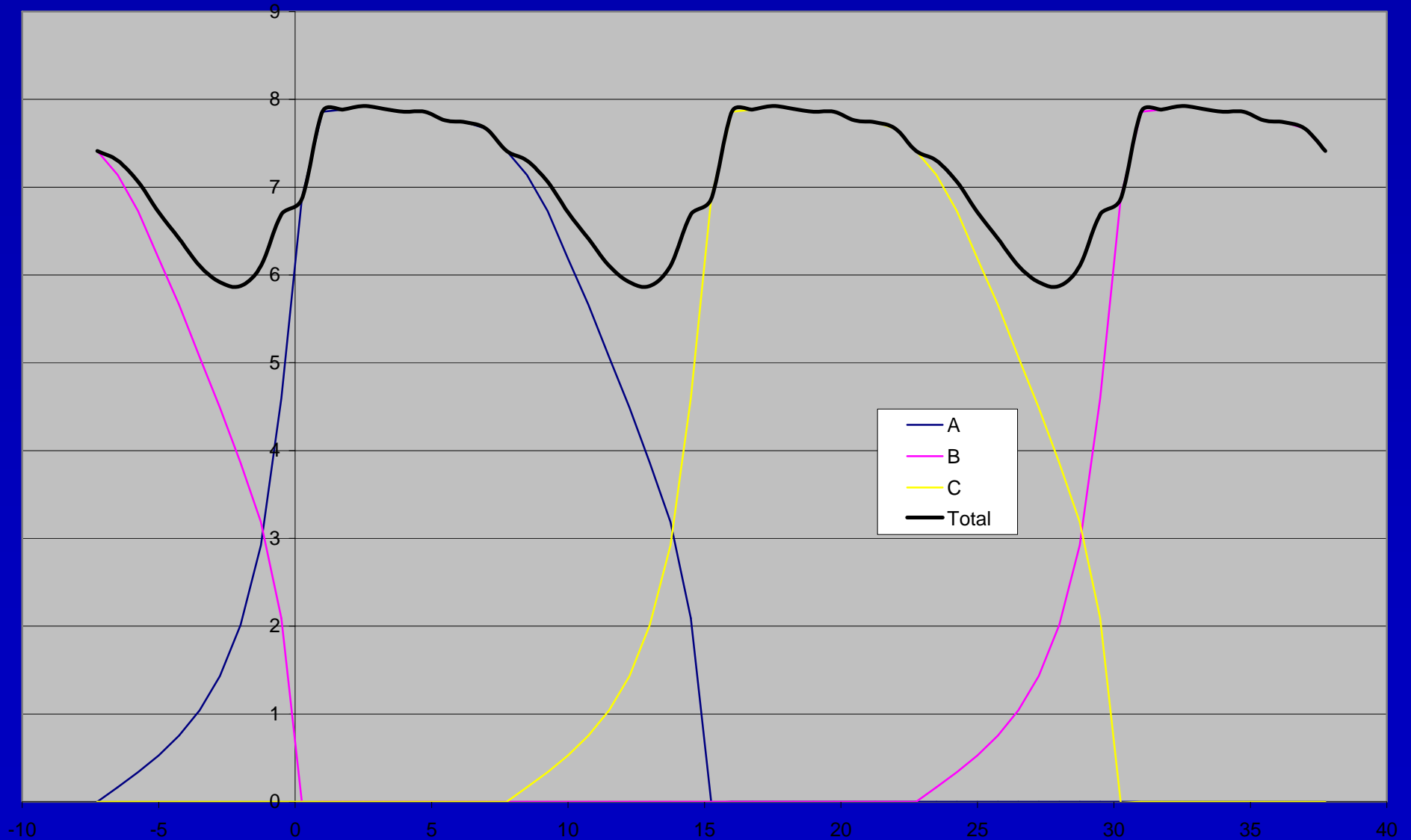
Summary so far...

- Motor is a member of the family “variable reluctance motors” (fundamental torque-producing mechanism)
- Operated by switching phases on & off with respect to rotor angle – *hence “switched” reluctance motor”!*
- Torque is produced as a result of changing phase inductance with respect to rotor angle
- Energise phases over *rising inductance* region to yield *motoring* torque
- Energise phases over *falling inductance* region to yield *braking* torque

Practical operation of “real” SR motors

- 1-phase motor discussed so far produces torque only half the time (inductance rises over half a revolution)
 - special arrangements to ensure starting (e.g. parking magnet)
 - but good for high speeds (e.g. fans, vacuum cleaners etc)
- Poly-phase motors usual for industrial applications
 - typically two, three or four phases
 - allow starting and generate smoother torque
- Phases are energised so that they overlap
 - e.g. 120 electrical degrees spacing on 3-phase motor,
90 electrical degrees on 4-phase motor
- Discussion so far assumes phase currents can be switched on & off instantaneously
 - not true in practice
 - controller has a bit more “work” to do to allow for this....

Summation of torque in three-phase motor



Rise/fall times of current and magnetic flux are finite

- Rate of rise/fall of magnetic flux ϕ is finite, as dictated by Faraday's Law:

$$\frac{d\phi}{dt} = \frac{V}{N} \quad \text{where } V \text{ is applied voltage}$$

N is number of turns

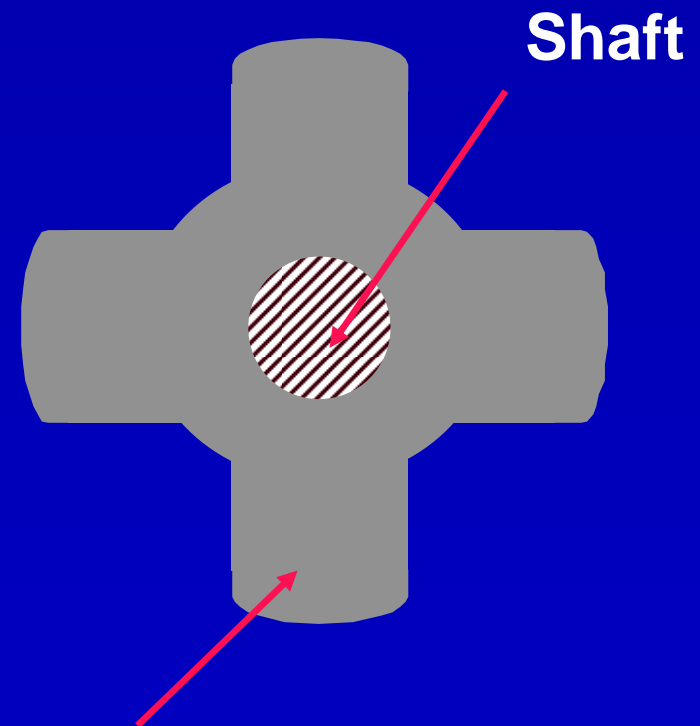
- Consider motoring operation:
 - 1) At BDC, there will be a delay before the current and magnetic flux reach their working values
 - 2) After switch off at TDC, flux and current will persist for a time
- Result would be fall in output and efficiency, because:
 - 1) would reduce the motoring torque component;
 - 2) would result in an additional braking torque component and also would prolong phase current (\Rightarrow more winding heat)
- Fortunately we can avoid this through cleverer control...

How is efficiency maintained at higher speeds ?

- At low speed, rise/fall times are negligible compared with time occupied by one electrical cycle
- As speed rises, delays become significant
- Compensate for delays by changing the rotor angles at which we switch-on and switch-off the phase excitation
 - switch on earlier, get flux to working value when inductance rising
 - switch off earlier, get flux down to low value before inductance falls
- Optimise switch-on and switch-off angles for best efficiency
- Very high efficiency possible over wide range of speeds and torques
- *Analogy -- advance in internal combustion engine*

“Simplest possible rotor”

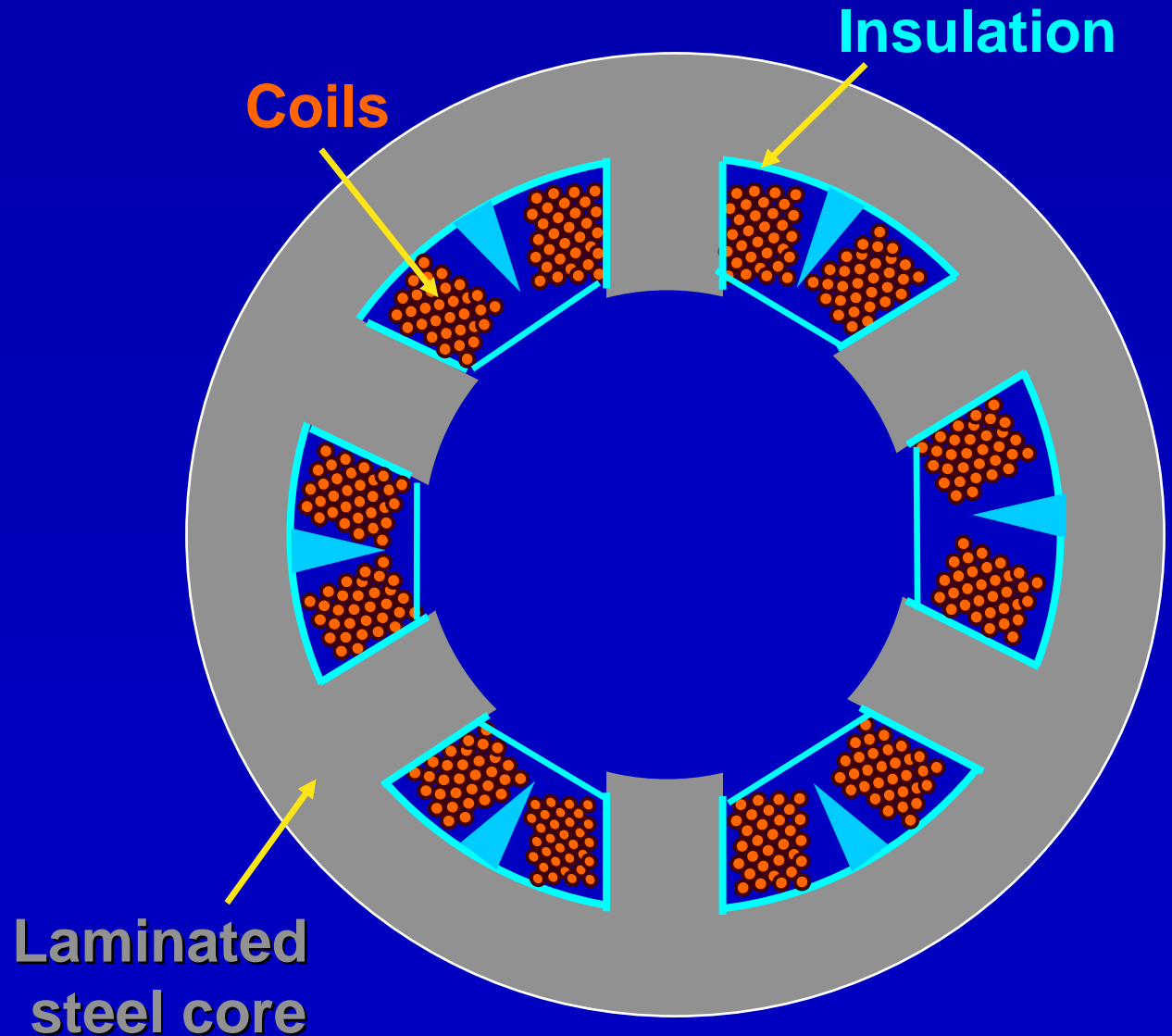
- No windings
- No commutator
- No rotor bars
- No magnets
- Minimal loss – “cool rotor”
- High speed and/or rapid acceleration no problem
- HIGHLY ROBUST



**Stack of steel laminations
(pressed or shrunk onto shaft)**

“Simple, robust stator”

- No overlap between phase windings – reduced risk of insulation failures
- Easily cooled
- Simple to wind, robust
- High dV/dt withstand
- Low capacitance to frame – reduced EMI



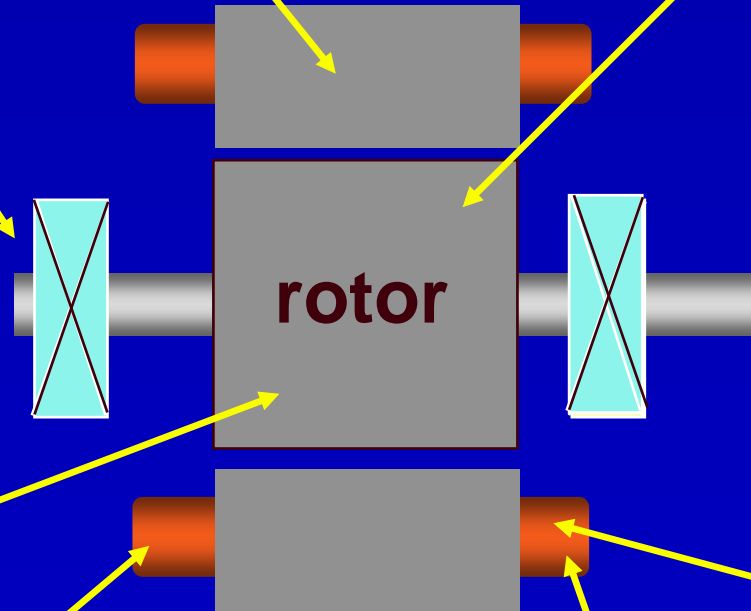
SR motor - inherent reliability

Simple thermal management

Cool bearings

Cool rotor

High dV/dt withstand
Lower capacitance to frame reduces RFI



Simple rotor:

- No windings
- No conductors
- No magnets
- No commutator

Mechanically Robust

No phase overlaps

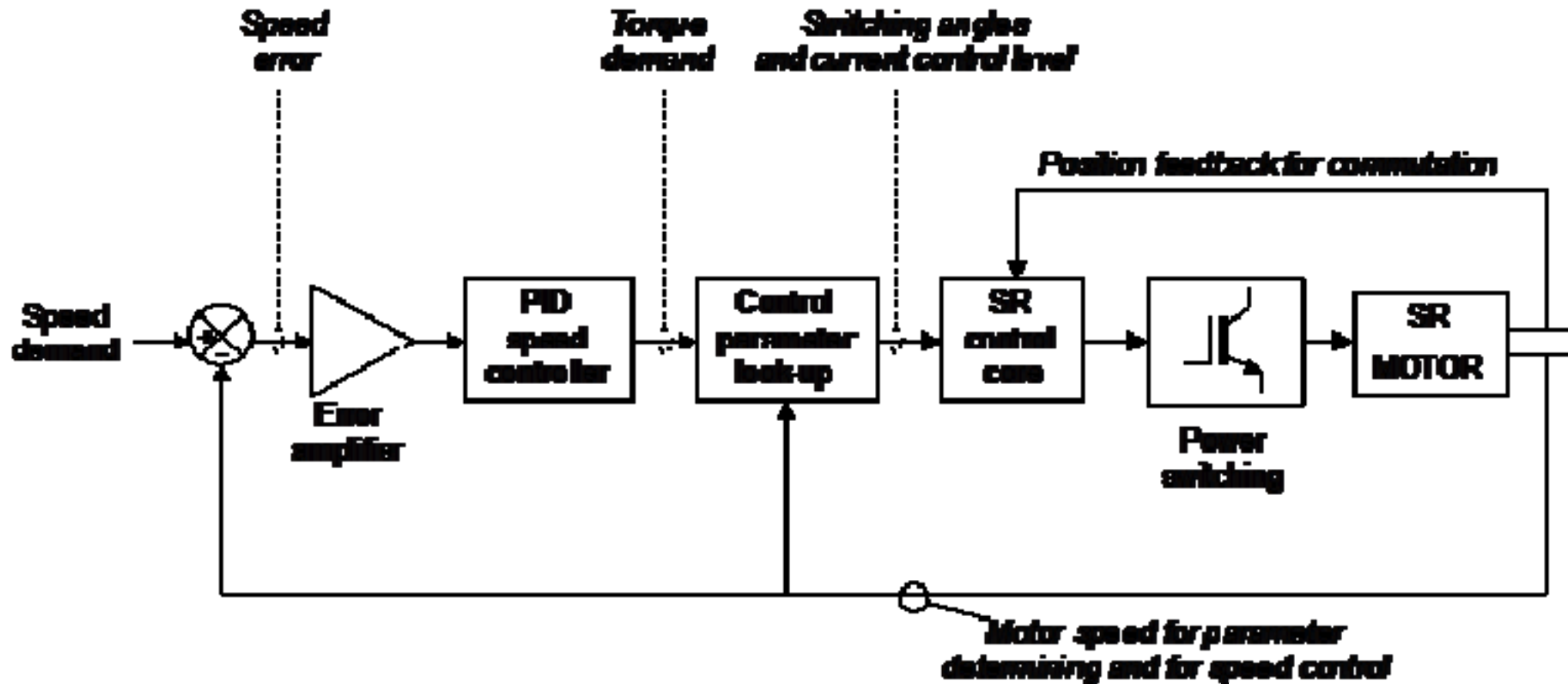
Short winding overhangs

- Lower hot spots
- Less movement

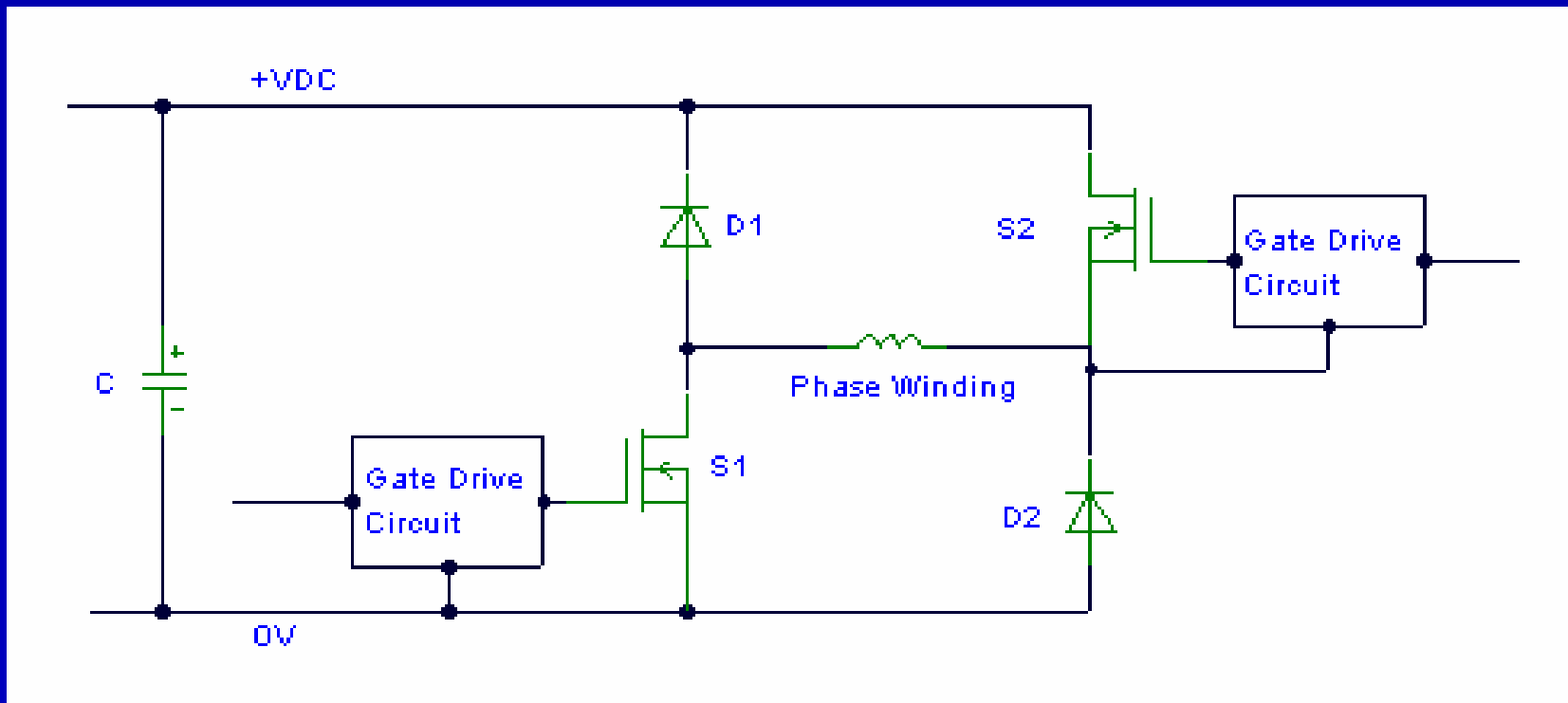
Key advantages of SR motor construction

- Brushless motor
- Simple laminated iron construction with salient poles
 - No rotor bars, no windings on rotor, no magnets
 - One simple coil per stator pole (may be pre-wound on bobbin/former)
- Ease of thermal management
 - losses concentrated in stator
 - cool rotor means improved bearing life
- High overload torques readily achieved (e.g. 1000%)
- Low rotor inertia inherent in geometry
- Short end-windings - good use of active material
 - flexible aspect ratio, high performance “pancake” motors possible

SR Drive[®]: typical control system architecture

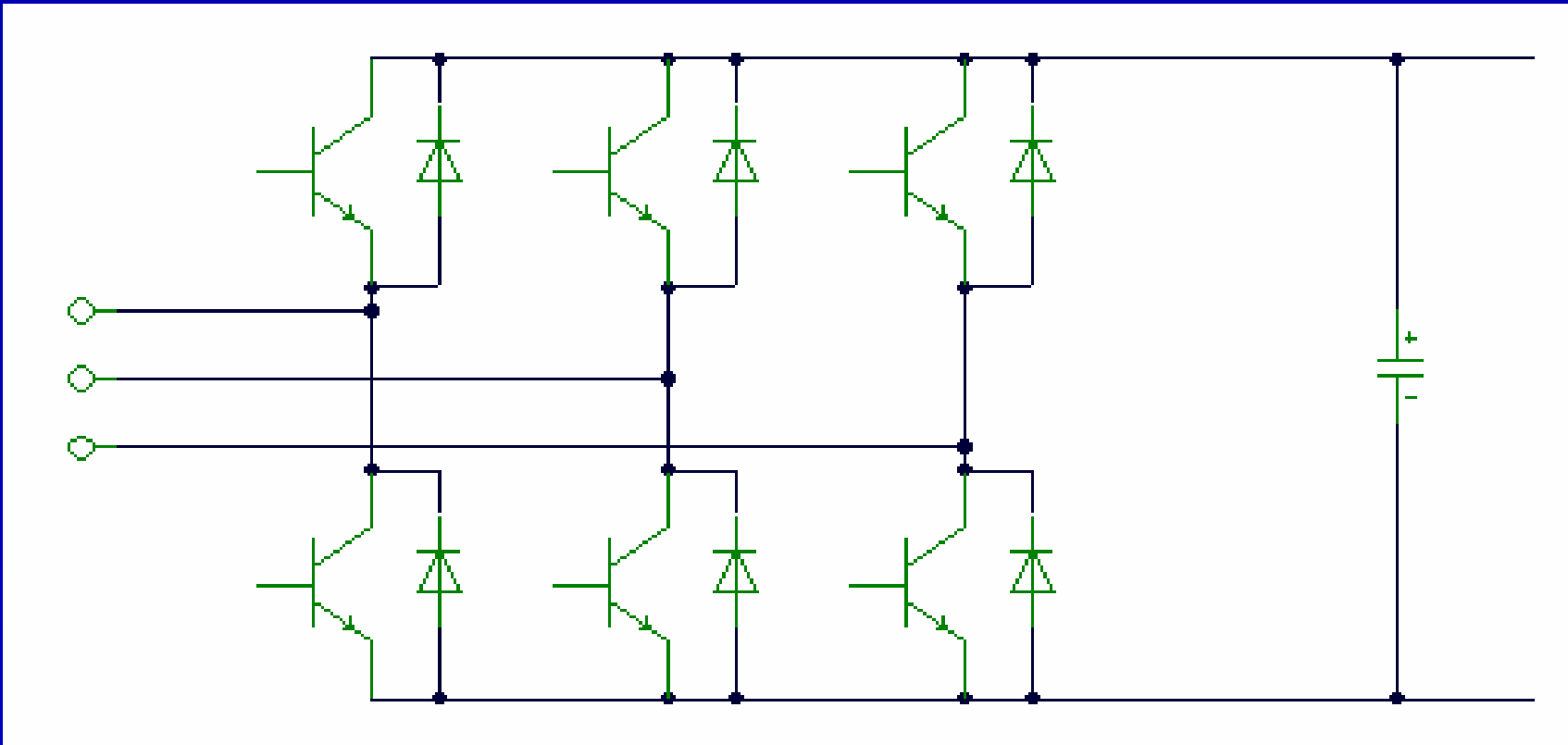


SR power converter “phase leg”



Semiconductor “switches” used, e.g. IGBT, GTO thyristor

3-phase inverter for PM and AC motors - for comparison

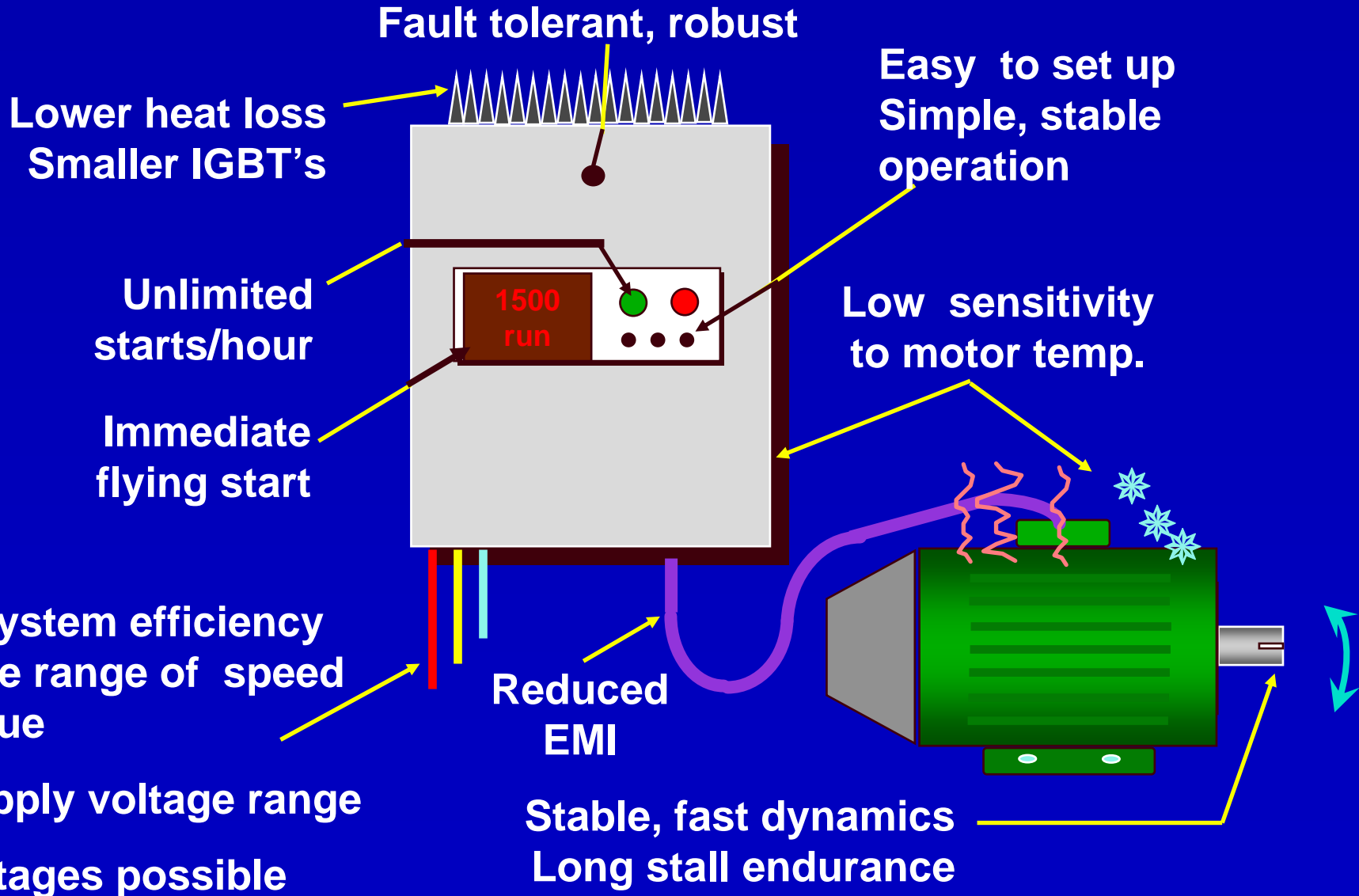


Note transistor switches are in series across power supply (= shoot-through possibility) and that they are in parallel with freewheel diodes (= dV/dt stress on switches)

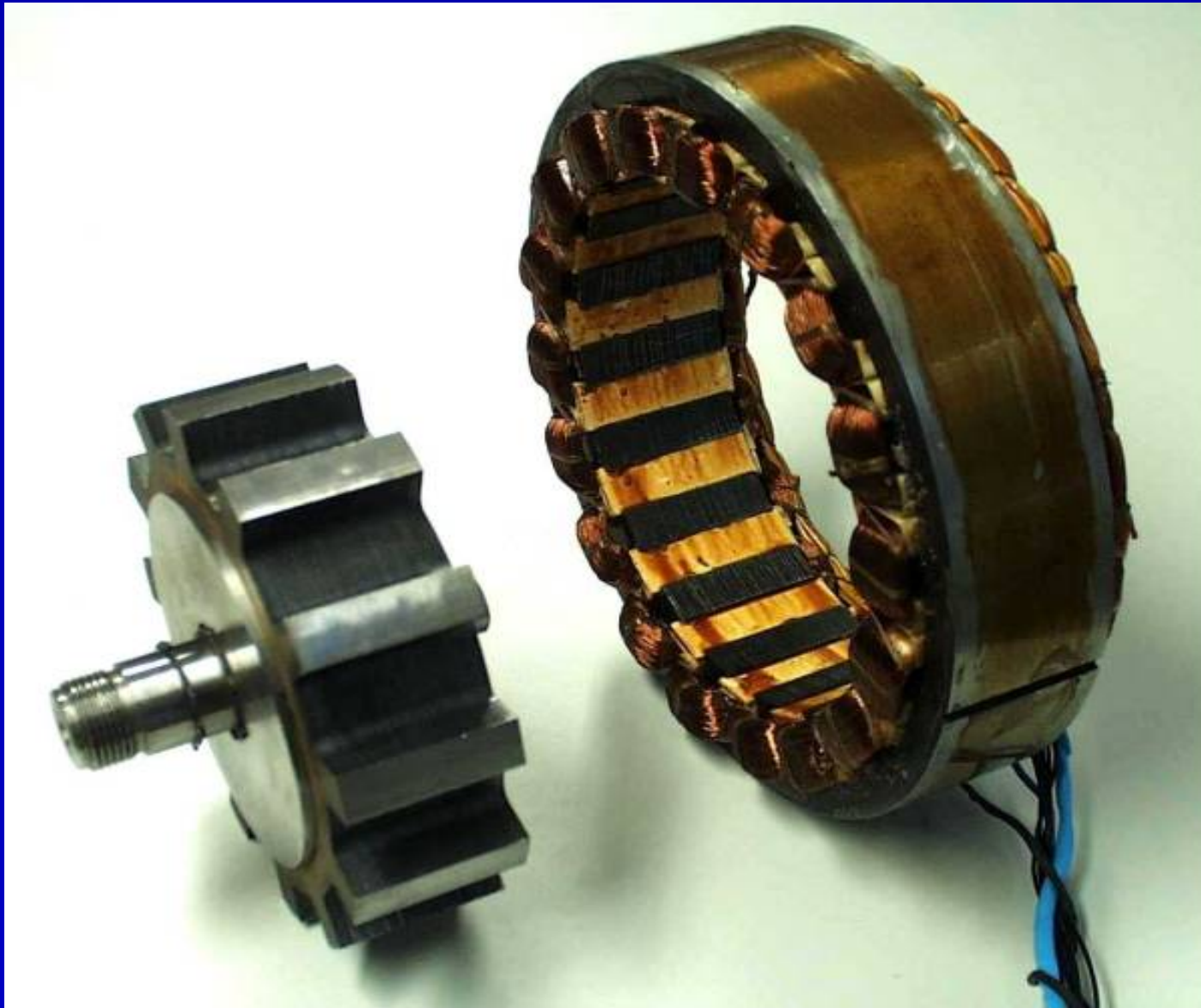
SR power electronics advantages

- **Winding in series with switches** – no “shoot-through” path
 - simplifies protection, enhances reliability
- **Lower power switch ratings compared with AC inverter**
 - high torque/amp inherent in SR motor
 - good high speed performance without reducing motor winding turns
- **Low switching frequency** – not synthesizing sinusoid
 - reduced switching losses and EMC
- **Unipolar currents in motor (even when regen. braking)**
- **Operation at “medium voltages” (e.g. 3.3kV AC) simplified by “stacking” converters (difficult in inverter)**
- **Switches are not subjected to reverse recovery transient voltage of freewheel diodes (unlike inverter)**
 - simplifies gate drive requirements

SR controller advantages



SR Stator and Rotor

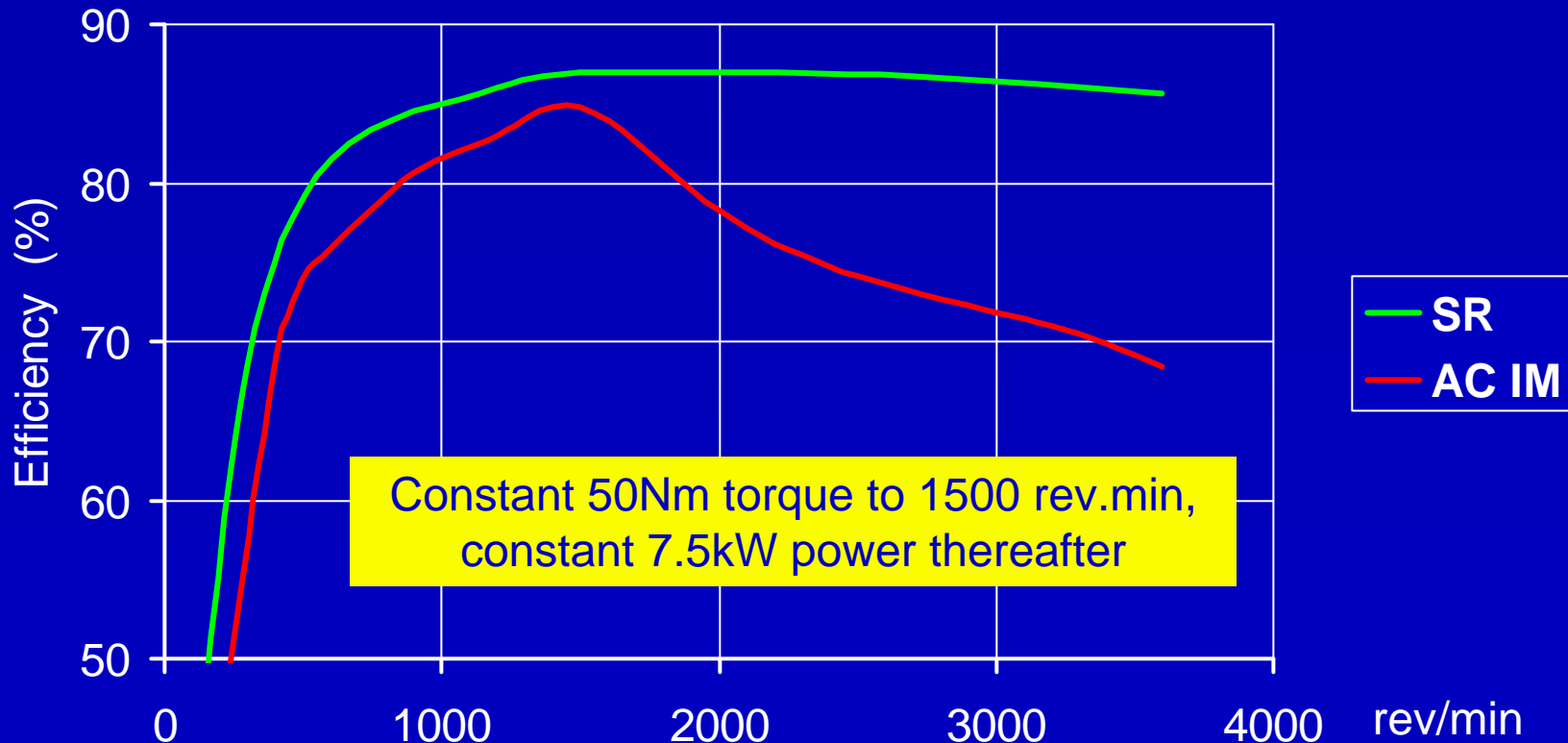


S R Drive® control system

- **Direct torque control via current and commutation angles**
 - Constant (controlled) torque operation possible
 - Optimised efficiency for wide range of torque & speed
 - Ability to tailor torque-speed envelope to suit application
 - Easy to use, only simple parameter set necessary (like DC drive)
 - but highly flexible, programmable control available if desired
- **Sensorless control now available if appropriate**
 - encoder often used (sim. to BPM & vector controlled IM)
- **Robust and fault tolerant**
 - rapid load changes and supply disturbances not a problem
 - fault diagnostics excellent
- **Acoustic noise control possible through electronic means**
 - significant IPR held here
 - also addressed through proper understanding of machine design

System efficiency: SR vs. vector AC motor @ 7.5kW

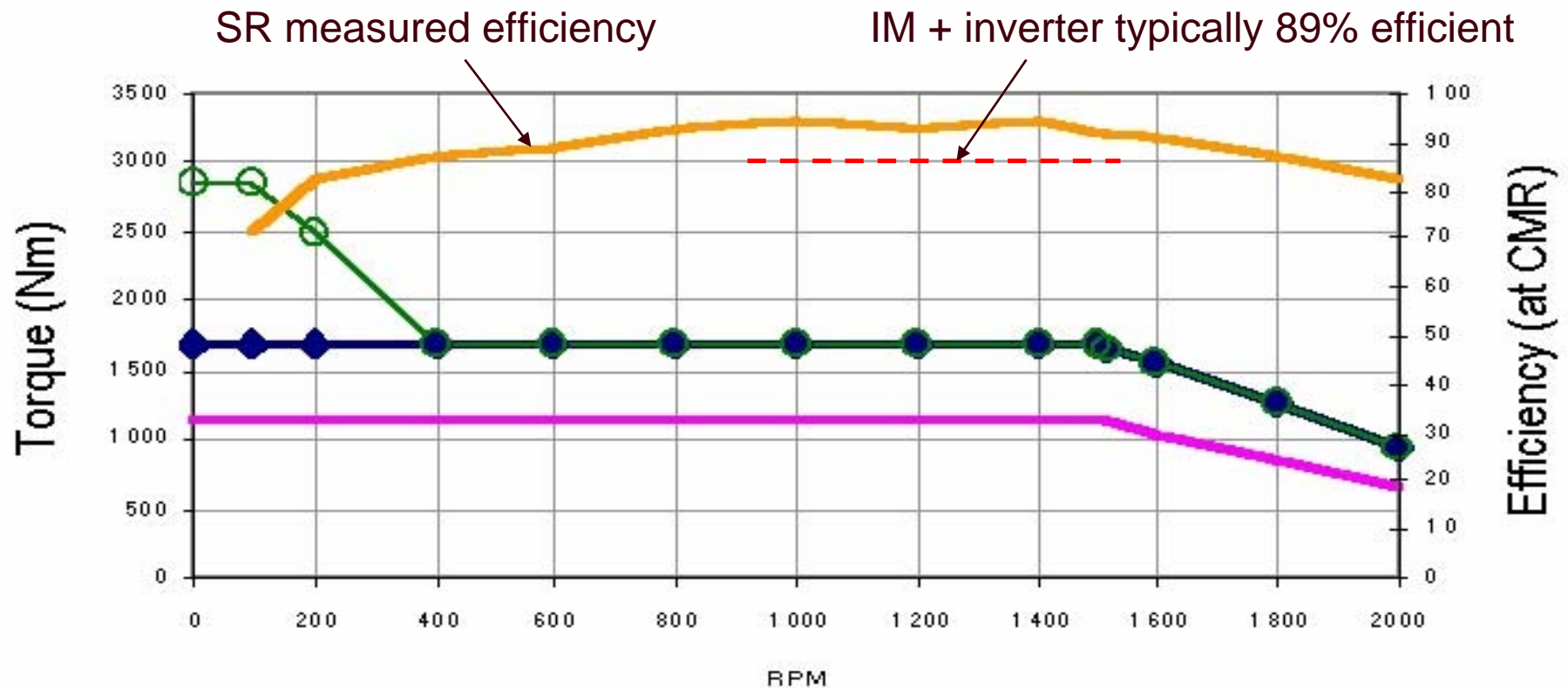
Same TEFC frame, IEC 132. Same switches, 50A IGBT. Full load torque



- SR efficiency is nearly flat over most of the working range
- Efficiencies & “flatness” maintained for torque values down to low levels

SRDML Diamond Drive torque and efficiency

180kW Diamond Drive Torque / Efficiency Graph



MAX TORQUE CMR TORQUE OPTIONAL HIGH STARTING TORQUE EFFICIENCY

Remarkably constant efficiency under varying load: e.g. IEC D250 motor (90kW)

Drive system comprising motor type 03-00017 operated with controller 02-00017
Measured system efficiency plotted vs. speed at 380V AC
SR Drives Manufacturing Ltd

